



# ***The Primary Design of Spoke014 cavity***

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## ***I. Introduction***

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## ***The requirements and parameters***

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- $\beta=0.14$
- The beam power per cavity: 5 kW.
- The diameter of beam tube: 50 mm.
- Antenna coupler is preferred. The position is perpendicular to the spoke, just as SSR1.
- The input coupler is a 50-ohm coaxial structure. Inner conductor diameter: 33.4 mm; Outer: 76.8 mm (**78.4 mm in SSR1**).
- $Q_e \sim 5.6e5$
- $E_{acc}$  (operating): 6~7 MV/m



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I. Introduction

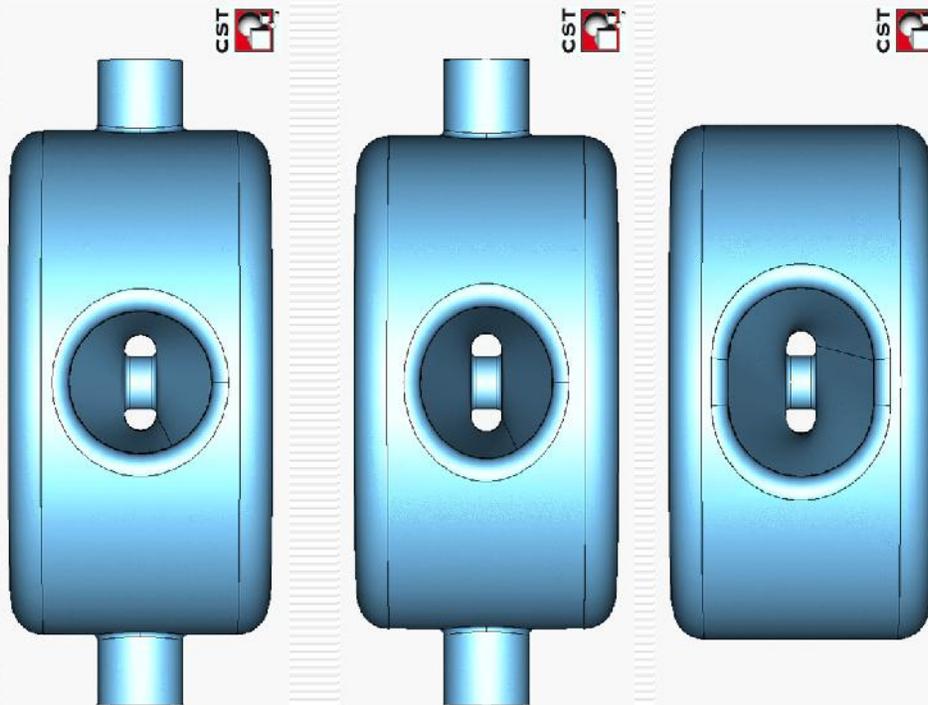
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# The cross section of spoke



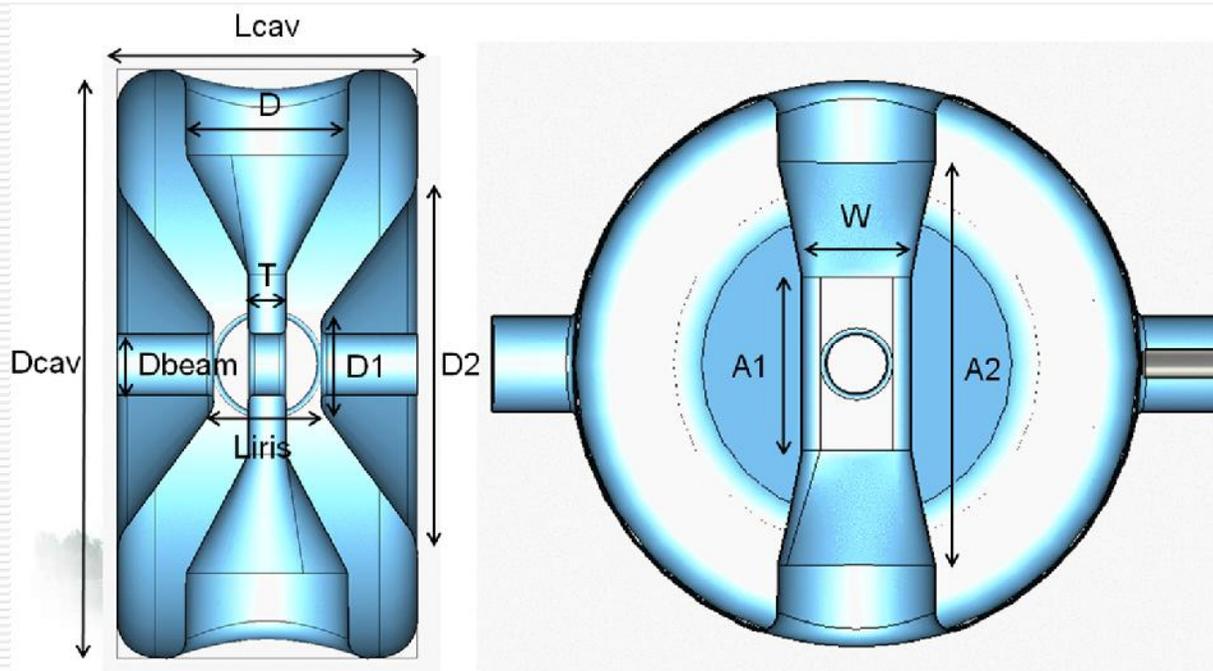
- 3 types of cross section:
- The left shape is round.
  - The middle shape is ellipse.
  - The right shape is racetrack.

The results of MWS show that: the  $B_{peak}/E_{acc}$ ,  $E_{peak}/E_{acc}$ ,  $R/Q_0$  and  $G$  of the middle type perform best. So the middle type has been adopted.

	Left	Middle	right
$G (\Omega)$	69	74	72
$R/Q_0 (\Omega)$	117	124	118
$E_{peak}/E_{acc}$	3.90	3.48	3.39
$B_{peak}/E_{acc}$ (mT/(MV/m))	4.41	3.94	4.23

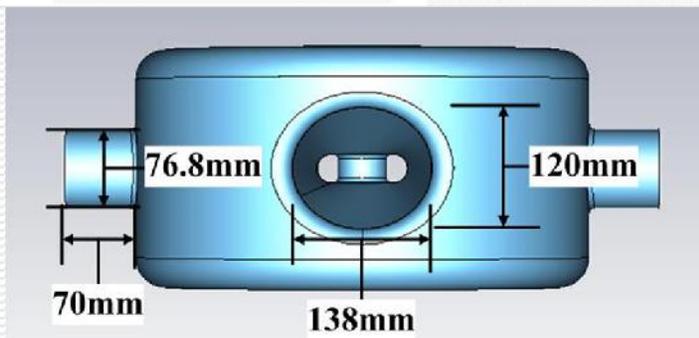


# Geometry parameters



Main parameters:

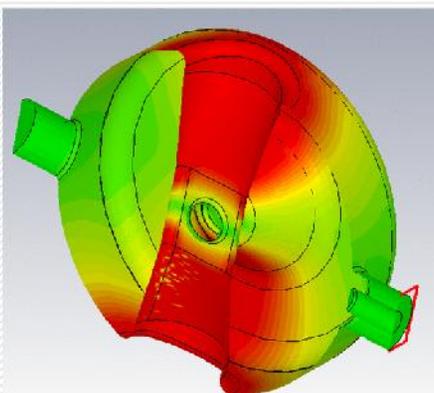
- $L_{cav}$ : 240 mm, cavity
- $L_{iris}$ :  $2\beta\lambda/3=86$  mm, iris to iris length
- $W$ : 109 mm, spoke width
- $T$ : 29 mm, spoke thickness
- $D_{beam}$ : 50 mm, beam tube diameter



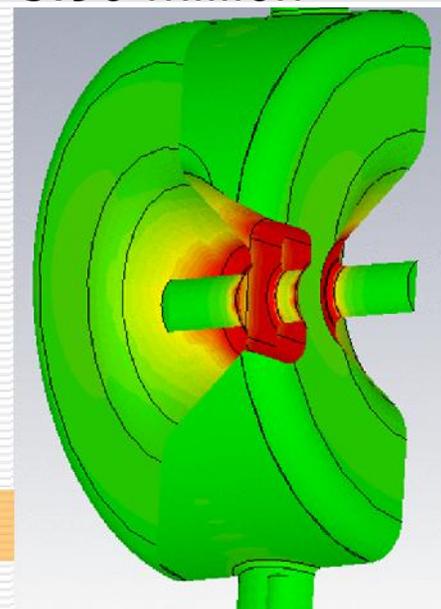


# The RF parameters

- RF simulation settings: 100 lines/wavelength, 3.96 million mesh cells.
- $E_{acc}$  is calculated with  $L_{iris} (2\beta\lambda/3)$ .
- $R/Q_0 = V_{acc}^2 / \omega U$



Magnetic field



Electric field

Frequency (MHz)	G ( $\Omega$ )	R/Q <sub>0</sub> ( $\Omega$ )	E <sub>peak</sub> /E <sub>acc</sub>	B <sub>peak</sub> /E <sub>acc</sub> (mT/(MV/m))	Q <sub>e</sub>
325.0	73	117	3.34	4.18	5.6e5



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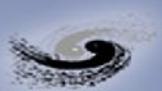
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## ***Mechanical design consideration***

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- ❑ We have little experience about the mechanical design of spoke cavity before.
- ❑ Solidworks and ANSYS are used to do the simulations.
- ❑ The material properties of niobium we used:  
Density=8560 kg/m<sup>3</sup>, Young's modulus=107 GPa, Poisson ratio=0.359, shell thickness=3.5 mm.
- ❑ There're two steps:
  - First, we use the cavity model without stiff ribs.
  - Second, we calculate it with stiff ribs (in progress).



## ***The spoke cavity without stiff ribs***

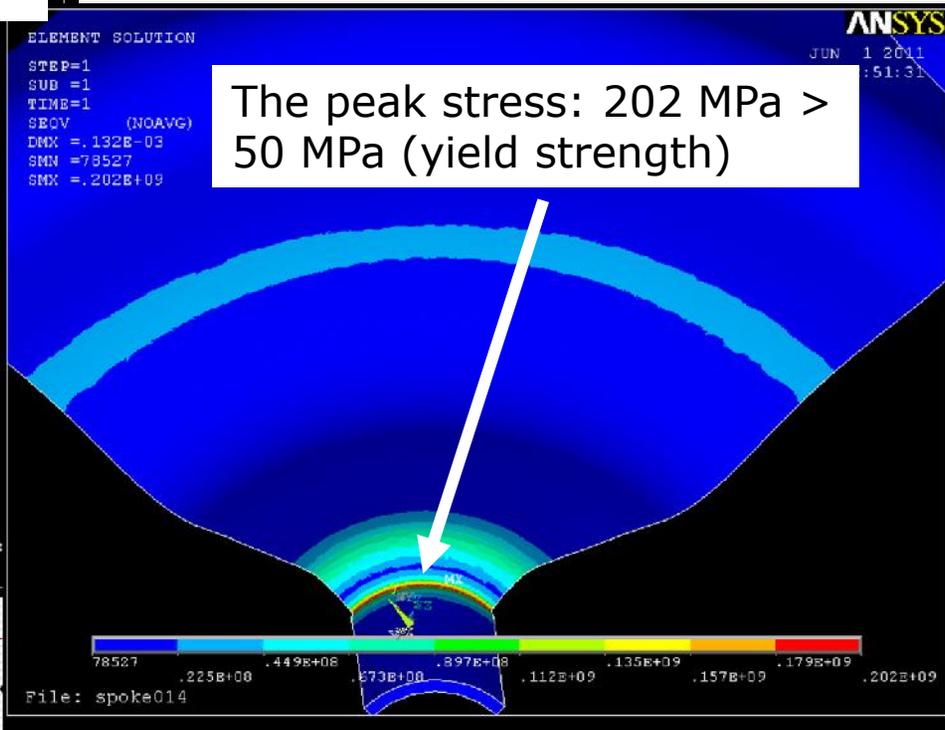
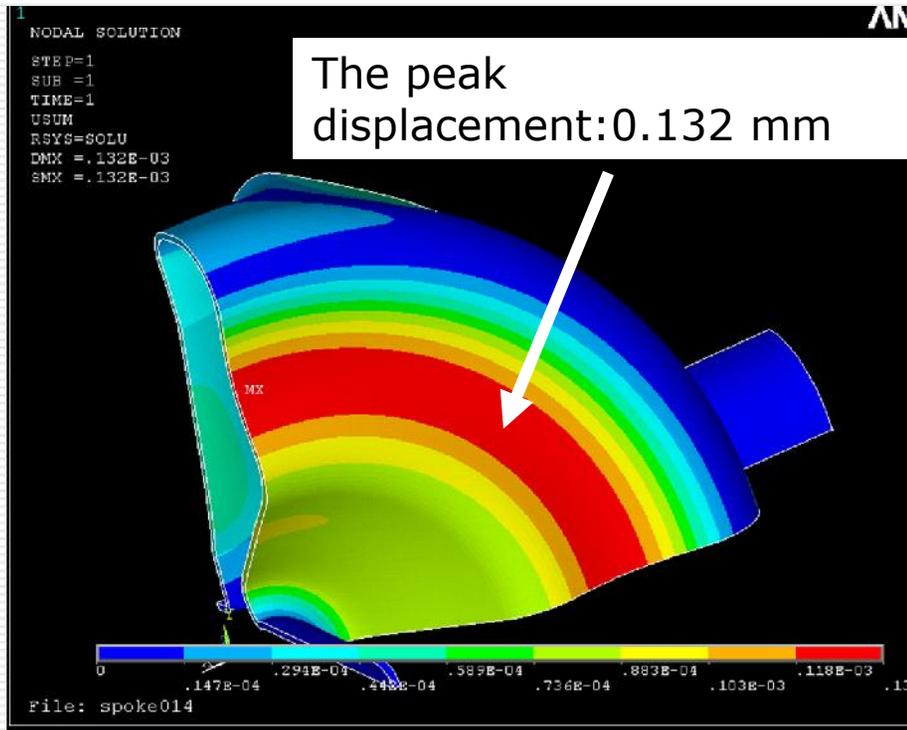
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- Simulation settings: 1/8 cavity, tetrahedral mesh cells, 270912 air cells, 68487 shell cells.
- Beam tube ports, coupler port and vacuum port are all fixed.
- The simulation includes:
  - External load
  - Tuning sensitivity (Beam tube ports free)
  - Lorentz force detuning (static)



# External load

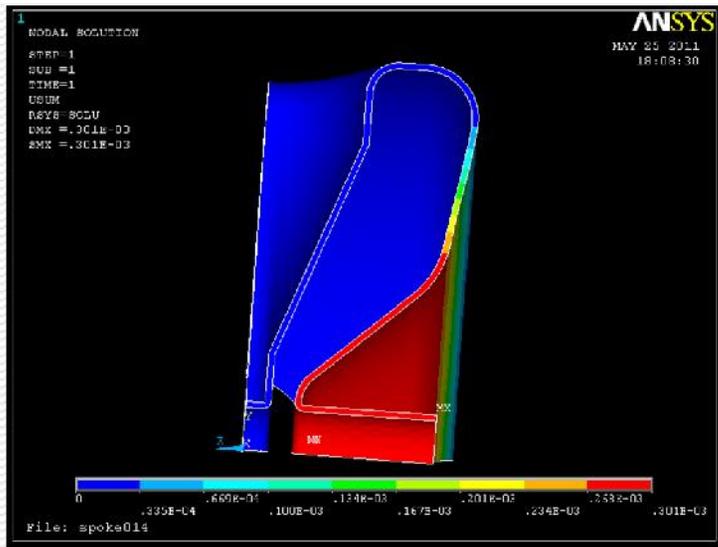
The external load: 1.18 atm (900 torr) → Frequency shift: -86.9 kHz



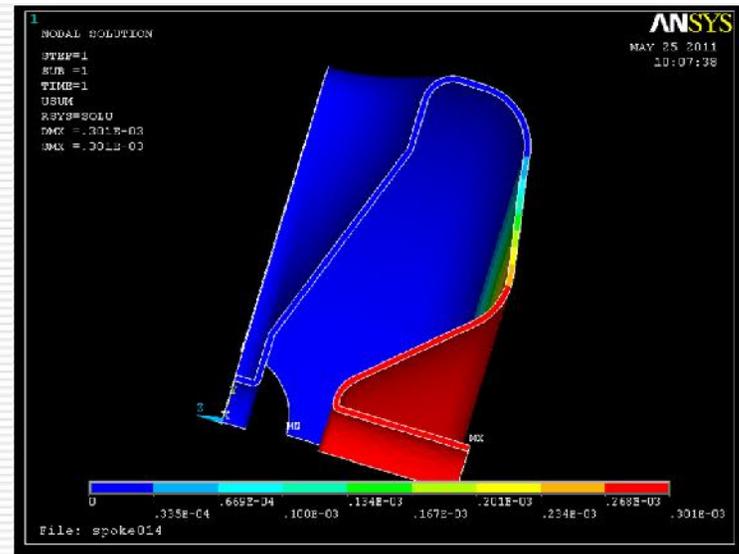


# Tuning sensitivity

Pulling: 980 N  $\longrightarrow$  cavity length: +0.6 mm  $\longrightarrow$  +617 kHz shift  
 Cavity length (beam tube flange): +1028 kHz / mm



Displacement of Pushing

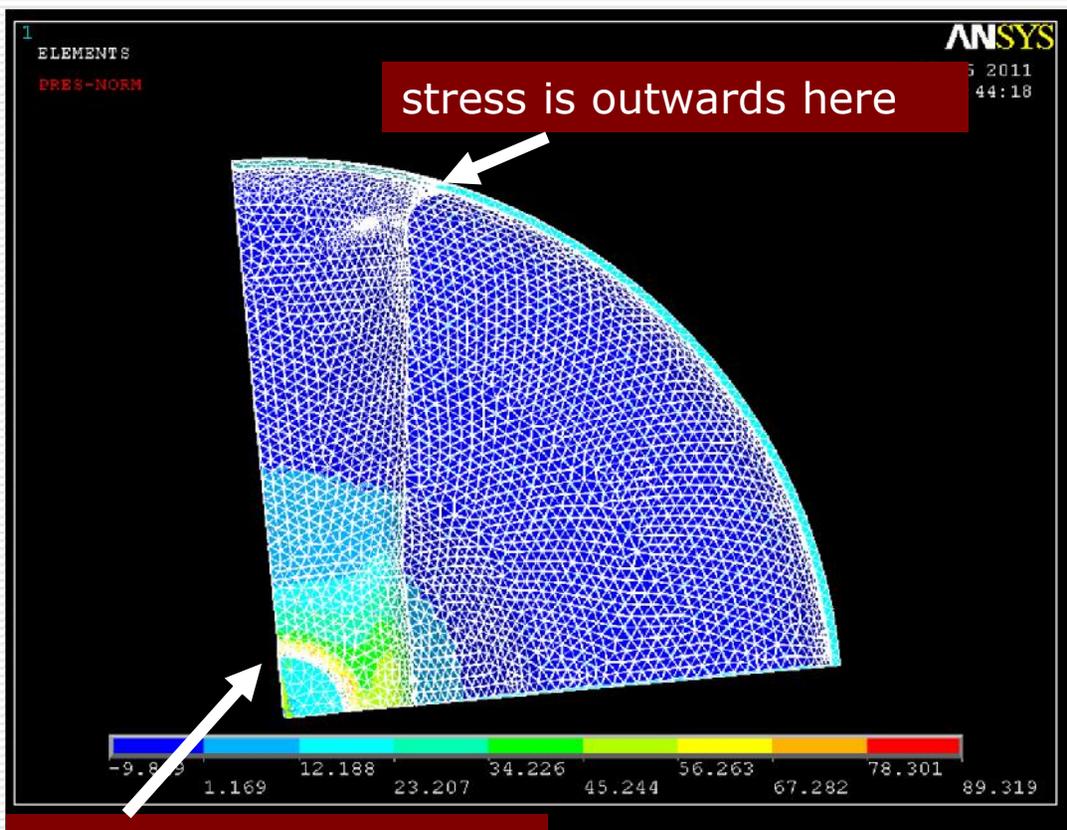


Displacement of Pulling

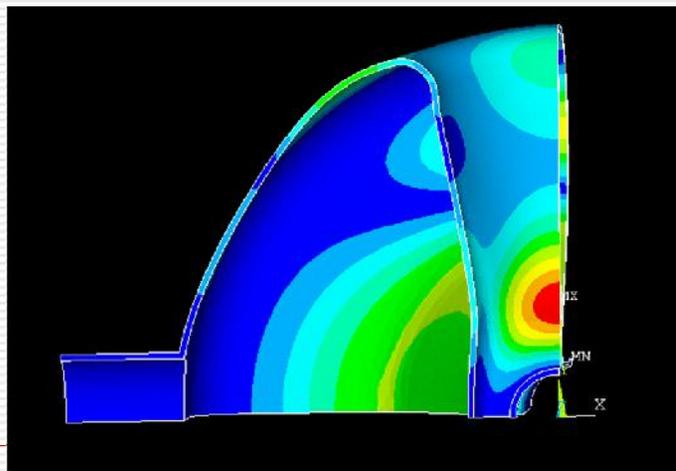


# Lorentz force detuning (static)

The Lorentz detuning coefficient:  $-6.33 \text{ Hz}/(\text{MV}/\text{m})^2$



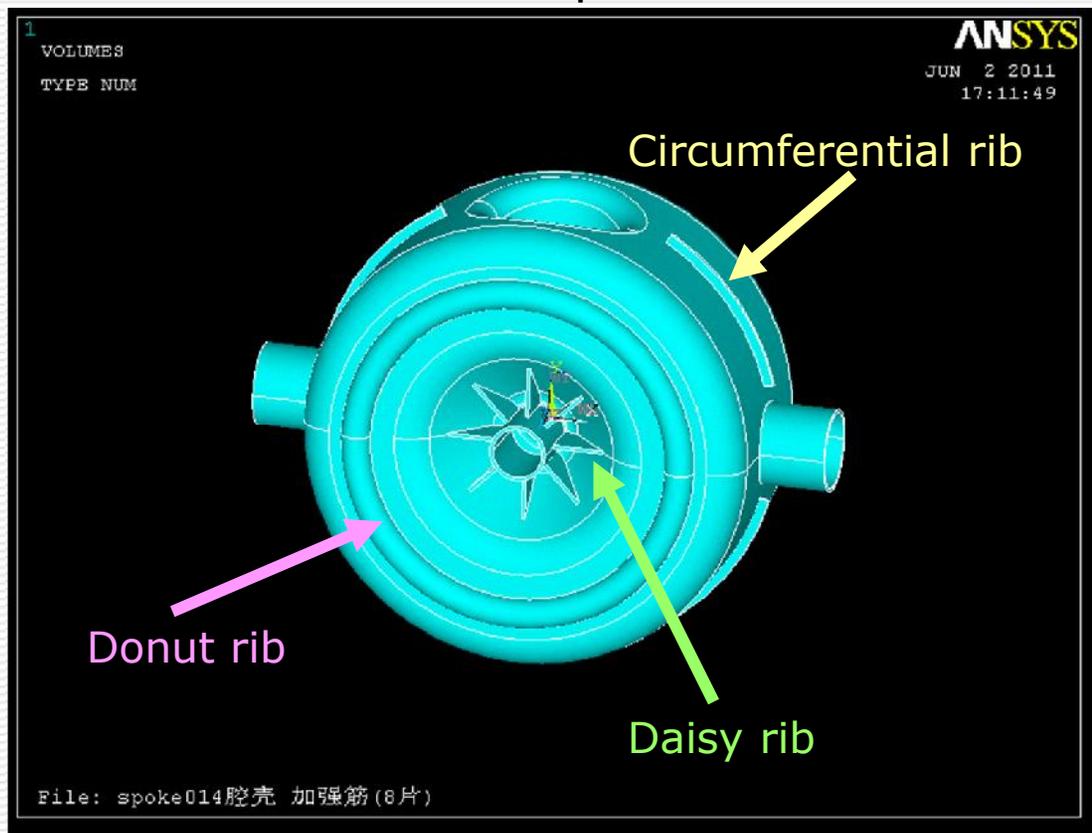
Displacement





## *The spoke cavity with stiff ribs*

- Simulation settings: 1/8 cavity, tetrahedral mesh cells, 270912 air cells, 83258 shell cells.
- The simulation process is the same as without stiff ribs.



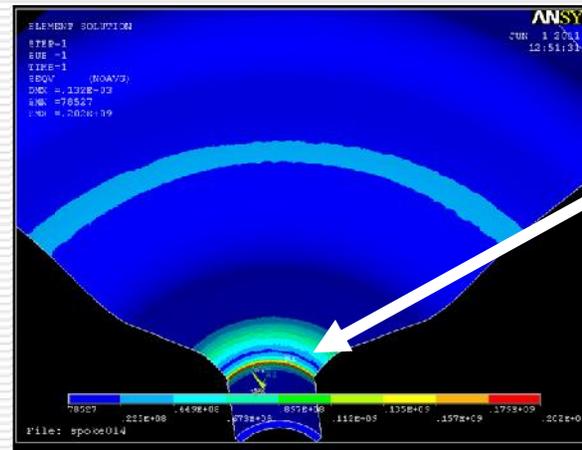
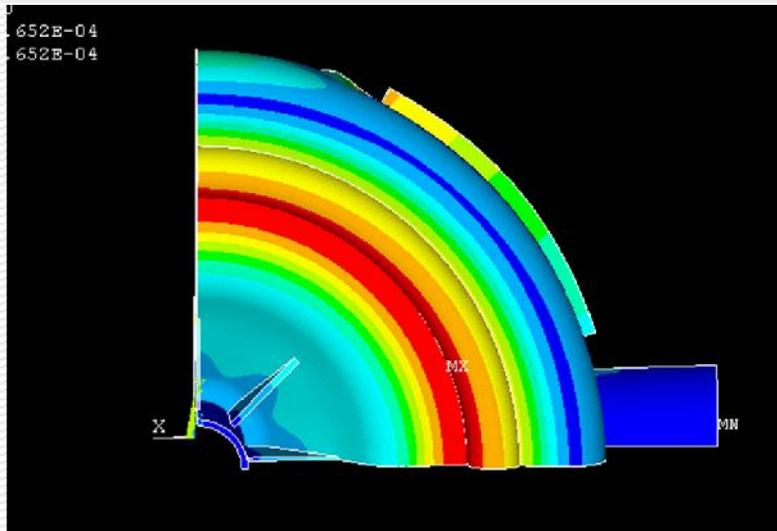
- 3 types of ribs are used.  
The thickness of ribs is 3.5 mm.
- two donut ribs
  - Four circumferential ribs
  - Eight daisy ribs



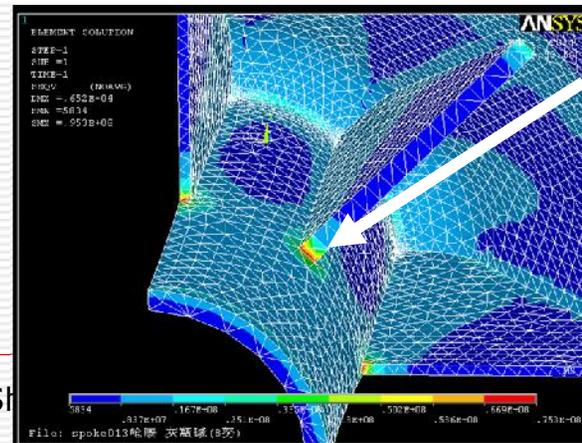
# External load with ribs

The external load: 1.18 atm (900 torr) → Frequency shift: -12.6 kHz

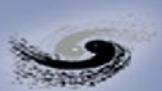
Peak displacement: 0.0652 mm, while 0.132 mm without ribs.



The peak stress: 202 MPa (without ribs)

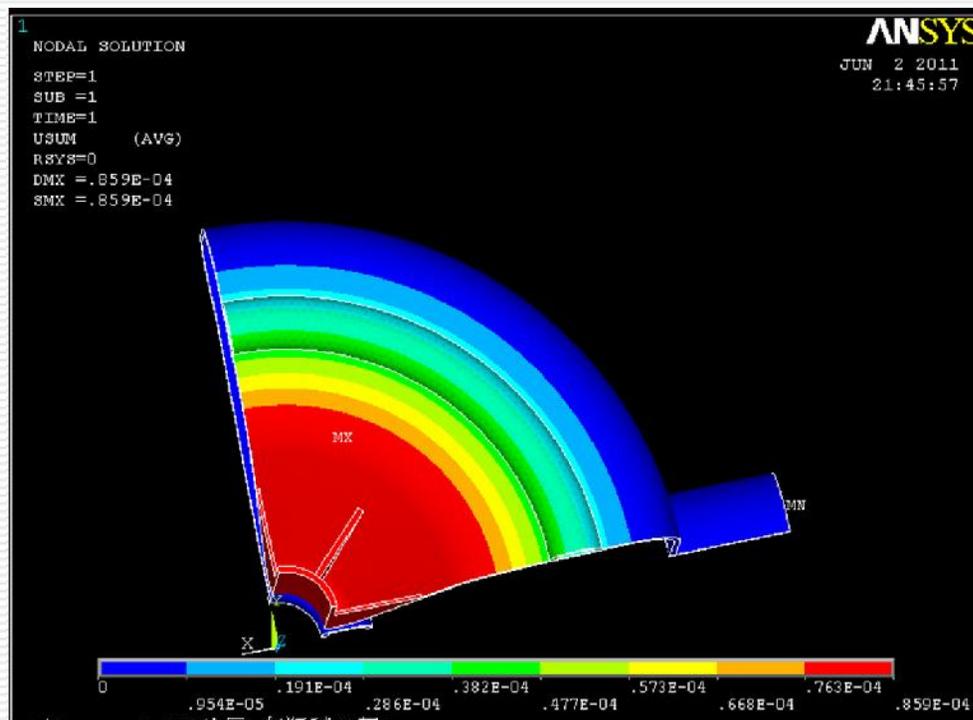


The peak stress: 75 MPa (with ribs)



## Tuning sensitivity with ribs

Pulling: 980 N  $\longrightarrow$  cavity length: +0.172 mm  $\longrightarrow$  +178 kHz shift  
 Cavity length (beam tube flange): +1040 kHz / mm

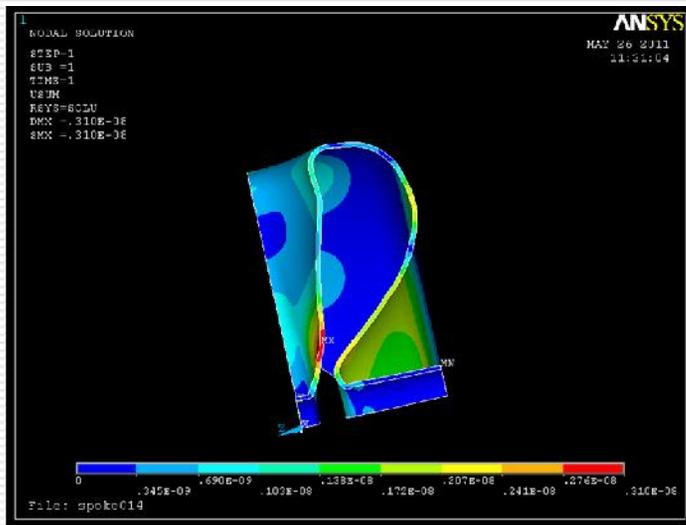


The peak stress: 9.9 MPa  
 Yield strength: 50 MPa  
 Tuning range:  $\pm 800$  kHz

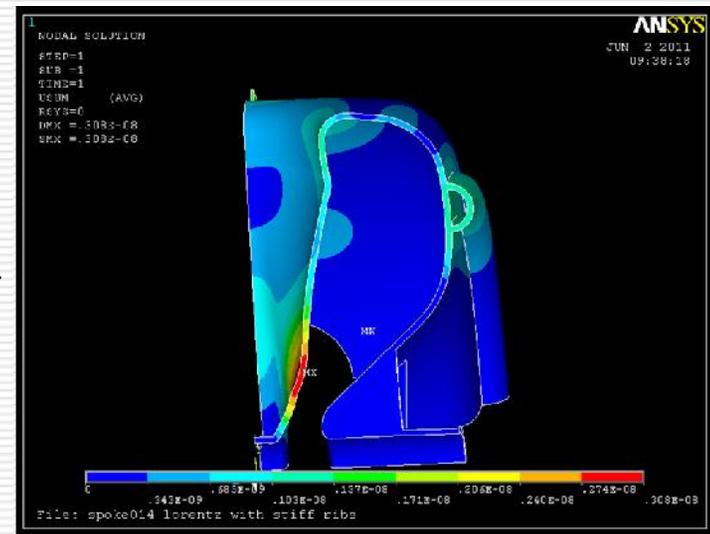
# Lorentz force detuning with ribs (static)

The Lorentz detuning coefficient:  $-3.79 \text{ Hz}/(\text{MV}/\text{m})^2$ , compared to  $-6.33 \text{ Hz}/(\text{MV}/\text{m})^2$  without ribs.

Displacement without ribs



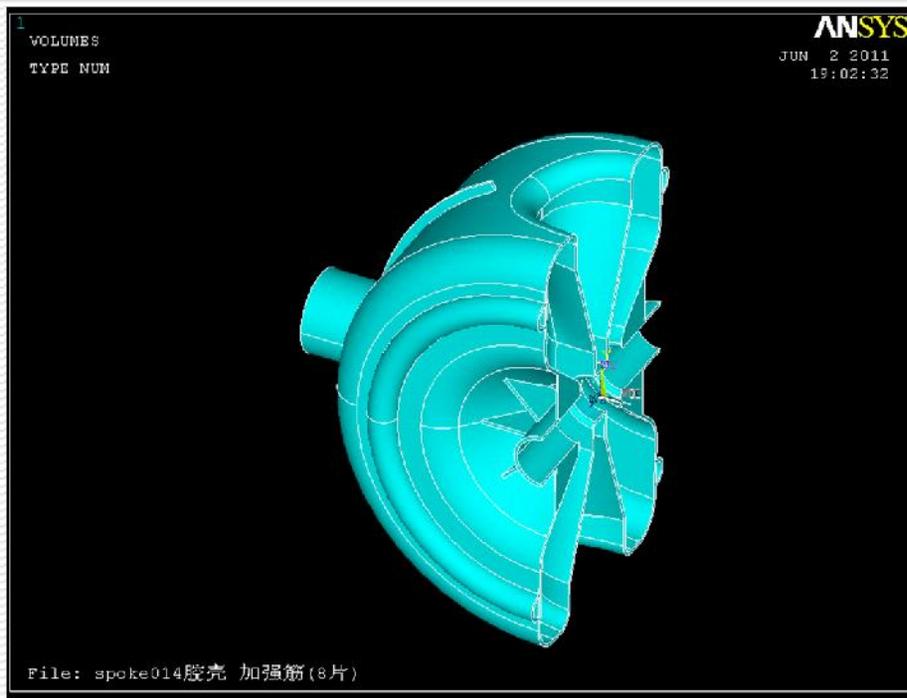
Displacement with ribs





# Microphonics

- The beam tube ports are fixed.
- 1/2 cavity, the first 5 mechanical oscillation modes calculated.



mode	f(Hz)
1	97
2	175.43
3	265.85
4	369.51
5	445.4



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## ***Summary and outlook***

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- ❑ The RF design of  $\beta=0.14$  spoke cavity has been finished.
- ❑ The mechanical design (with stiff ribs) is in progress now.
- ❑ Research of the cavity unit with tuner, coupler, helium vessel, etc, are the main work in future.
- ❑ Next, we will focus on  $\beta=0.12$  spoke cavity, whose beam aperture changes from 50 mm to 40 mm .



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# Thanks you!