

# Test Results With a Prototype Helical Kicker

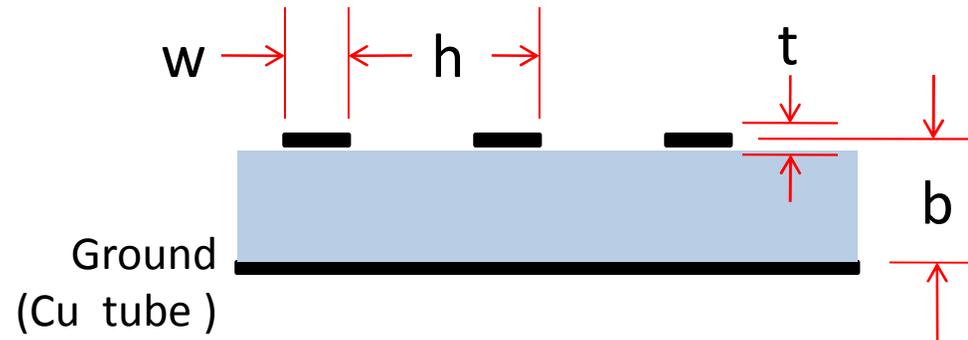
Greg Saewert

## Topics

1. Test results of 200  $\Omega$  helix
2. Future effort with helix
3. Helix temperature

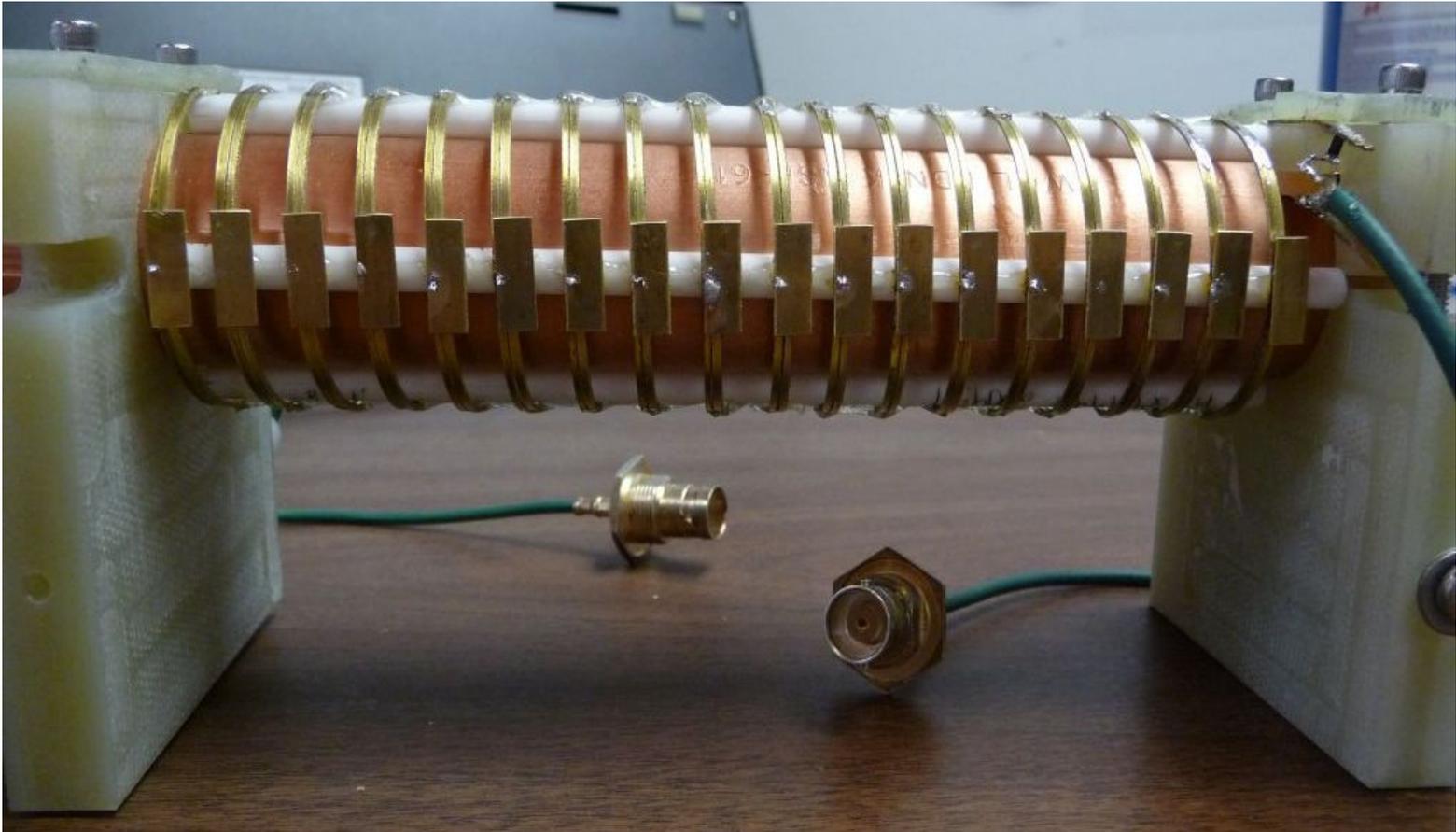
Project X meeting  
May 3, 2011

# Microstrip line dimensions



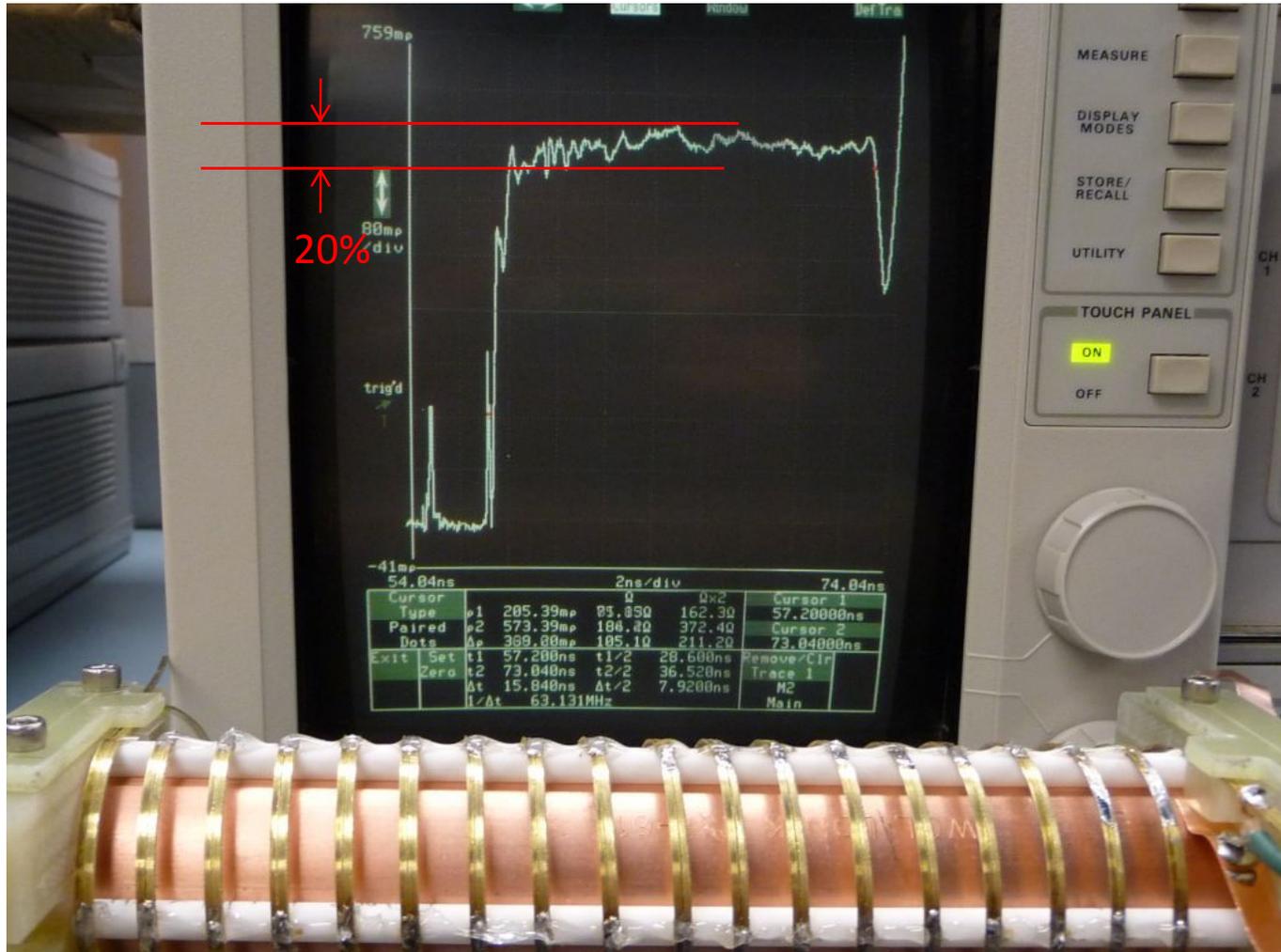
Characteristic impedance	$205 \pm 20 \Omega$ (measured)
Conductor strip dimensions ( $w \times t$ )	0.091 x 0.02 inch
Pitch ( $h$ )	0.333 inch
Strip height ( $b$ )	0.197 inch
Helix outer diameter	1.47 inches
Ground tube diameter	1.125 inches
helix length (18 turns)	6 inches

# Helical microstrip line

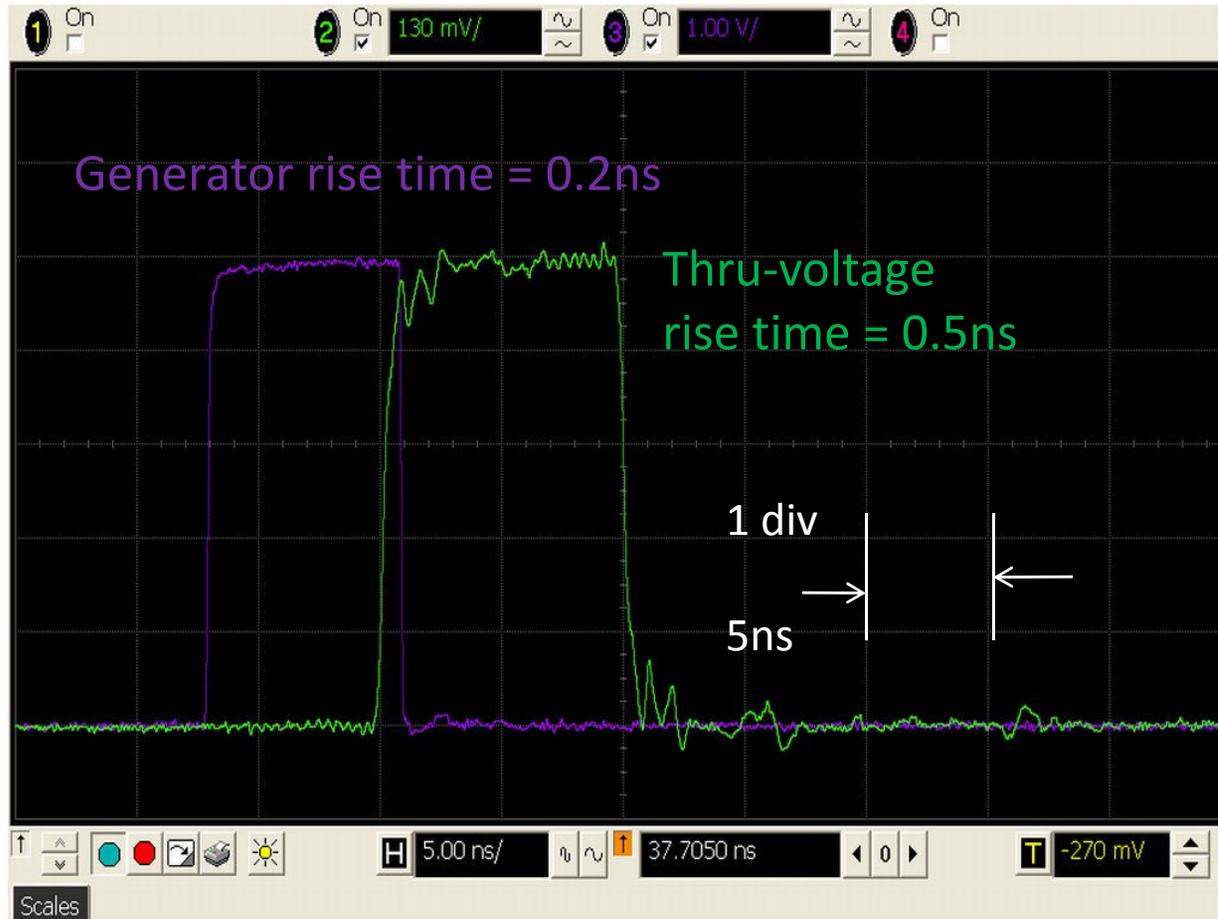


0.18 (W) x 0.50 (H) in. electrodes attached

# TDR impedance measurement



# Transfer Response (TD)



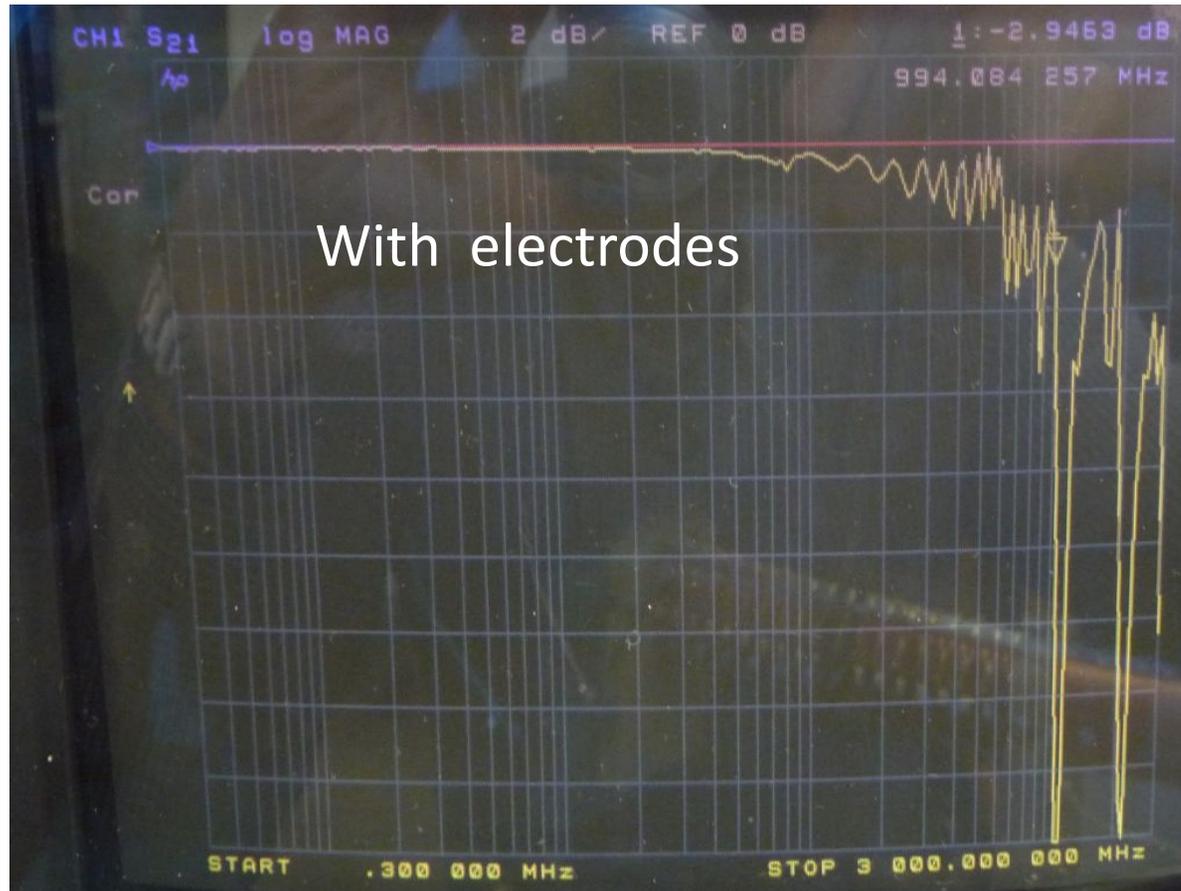
- 205 Ohm microstrip line is resistively matched to 50 Ohms, in and out
- .18 (W) x .50 (H) in. Electrodes are attached

# Network analyzer response (S21)



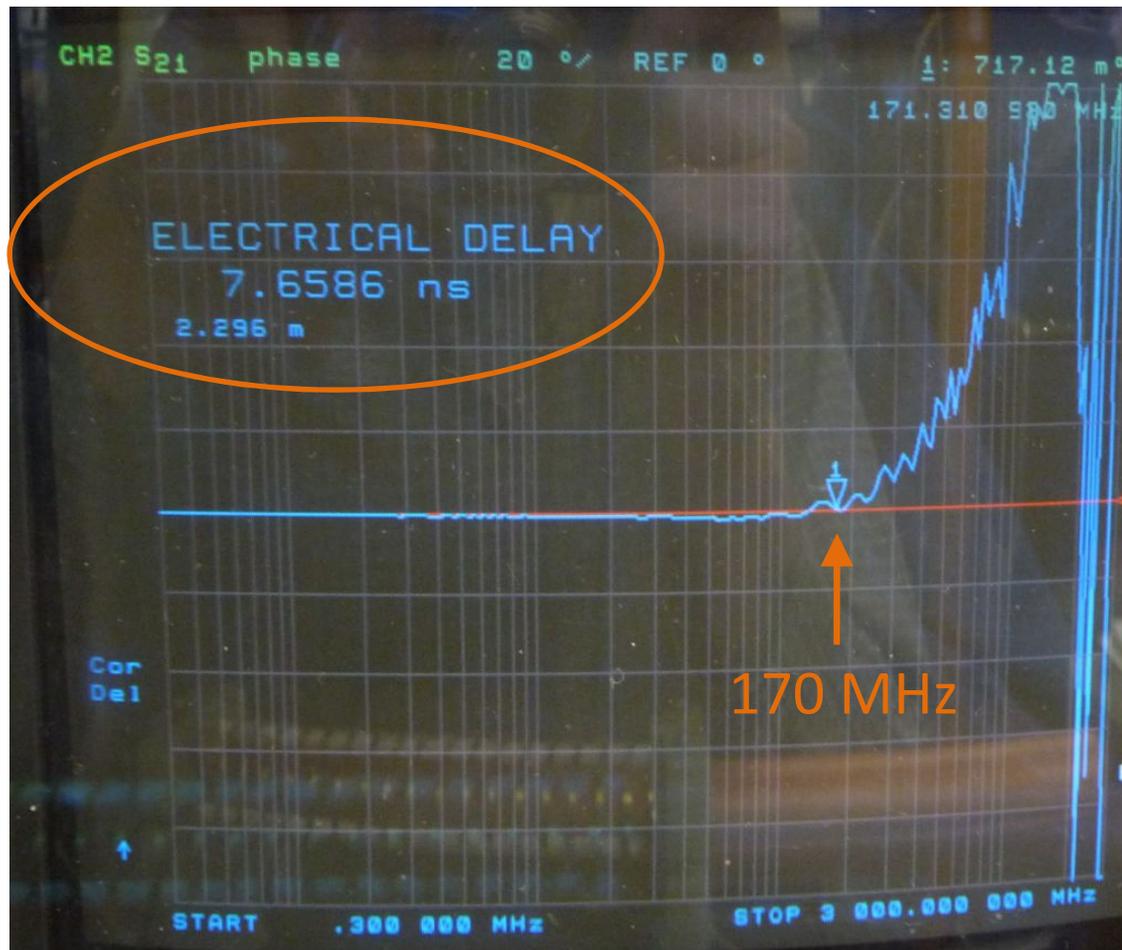
- Sweep range: .30MHz – 3GHz
- Vertical scale: 2dB/div
- Response remains below 3dB above ~800 MHz
- Matching resistor network and cable are calibrated out of the measurement

# Network analyzer response (S21)



- Sweep range: .30MHz – 3GHz
- Vertical scale: 2dB/div
- Response rolloff remains below 3dB above 900 MHz
- Fixture was calibrated out

# Network analyzer S21 phase response



- Sweep range: .30MHz – 3GHz
- Vertical scale: 20 deg/div
- Matching resistor network and cable are calibrated out of the measurement

# Observations & Conclusions

- Prototype construction suffered from dimensional irregularities
  - Strip width varies 12% along the length
  - Pitch varies +/-10% turn-to-turn
- Resulting impedance variations are 20% along the length
  - Some ripple is due to ceramic rod supports, though
- Electrode electrical effects are only above 700 MHz
  - Each is an impedance discontinuity
  - Electrode required size seems to be small enough to be tolerable
- Dispersion effects with 6" are enough to question longer version

# Design considerations

Using Valerie Lebedev's expressions from Project X Meeting, Nov. 3, 2010:

## Coupling coefficient

$$K_C \approx \ln\left(\sqrt{1 + (2b/h)^2}\right) / \ln\left(\frac{32b}{\pi w}\right), \quad w \ll b, h$$

## Dispersion

$$K_D \approx \sqrt{\epsilon} \frac{\omega}{c} \left[ 1 + 8K_C^2 \cos\left(\sqrt{\epsilon} \frac{\omega l}{c}\right) \right] \sin^2\left(\sqrt{\epsilon} \frac{\omega l}{2c}\right) \quad \begin{array}{l} l - \text{length of a single turn} \\ \epsilon - \text{is dielectric permittivity} \end{array}$$

## Coupling and dispersion for different 200 Ω helices

Z <sub>o</sub>	Gnd Tube OD	b	w	h	K <sub>C</sub>	K <sub>D</sub>
175	.75"	.125"	.10"	.222"	.1610	.063497
205	1.125"	.177"	.090"	.333"	.1227	.063568
200	1.5625"	.177"	.090"	.441"	.0831	.063257
200	1.825"	.177"	.090"	.500"	.0676	.063116
200	2.125"	.177"	.090"	.570"	.0546	.062994

ProjectX Meeting, May 3, 2011, Greg Saewert

## Further effort with helix microstrip line approach

- There is no compelling reason to stay with 1.125" size helix
- Design a larger helix for less dispersion
- Choose 2.125" OD copper ground tube
  - Stock size 2" copper tube
  - Electrodes will be 1.5 cm x 1.5 cm (sufficiently small?)
- Anticipate winding full .5 m

# Microstrip conductor temperature

- Copper skin depth at 80 MHz

$$\delta \approx 503 \sqrt{\frac{\rho}{\mu_r f}} \approx 7.3 \times 10^{-6} \text{ (m)}$$

$\rho$  – resistivity of copper  
=  $1.68 \times 10^{-8}$  ( $\Omega$ -m)

$\mu_r$  – relative permeability (=1)  
 $f$  – frequency (Hz)

- Resistance in one skin depth of the strip per unit length

$$R^* = \frac{\rho}{A_X} = \frac{1.68 \times 10^{-8}}{7.3 \times 10^{-6} \cdot .09 \cdot .0254} = 1.0 \text{ (}\Omega/\text{m)}$$

$A_X$  – skin effect cross sectional area ( $\text{m}^2$ )

- Power dissipated in the microstrip

$$P^* = I^2 \cdot R^* = 1.0 \text{ (W/m)} \quad I = \frac{400 \cdot .50 (V_{rms})}{200 (\Omega)} = 1.0 \text{ (A)}$$

- Temperature of the conductor is derived from

$$P^* = \sigma A_S (T^4 - T_0^2)$$

$\sigma$  – Stefan-Boltzmann constant  
=  $5.67 \times 10^{-8}$  ( $\text{W}/\text{m}^2/\text{deg}^4$ )

$A_S$  – conductor surface are =  $5.58 \times 10^{-3}$  ( $\text{m}^2$ )

$T^4$  – conductor temp. (K)

$T_0^4$  – ambient temp. (298 K)

# Microstrip conductor temperature – cont.

- Conductor temperature

$$T = \left( \frac{P^*}{\sigma A_S} + T_0^4 \right)^{\frac{1}{4}} = 324 \text{ (K)} = 51^\circ \text{C}$$

- Compare with a 50 Ohm helix

$$T = \left( \frac{16}{\sigma A_S} + T_0^4 \right)^{\frac{1}{4}} = 492 \text{ (K)} = 219^\circ \text{C}$$

End