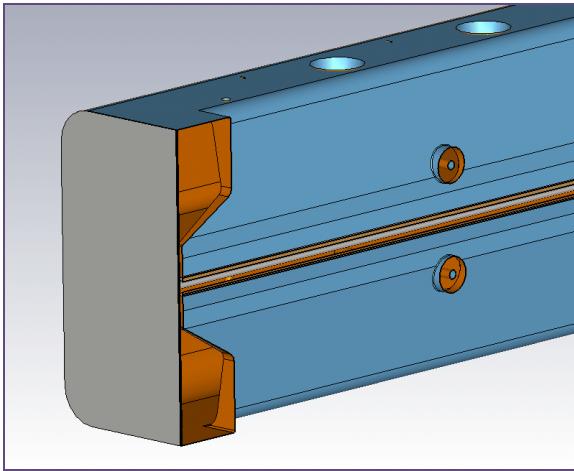


PXIE RFQ end-walls

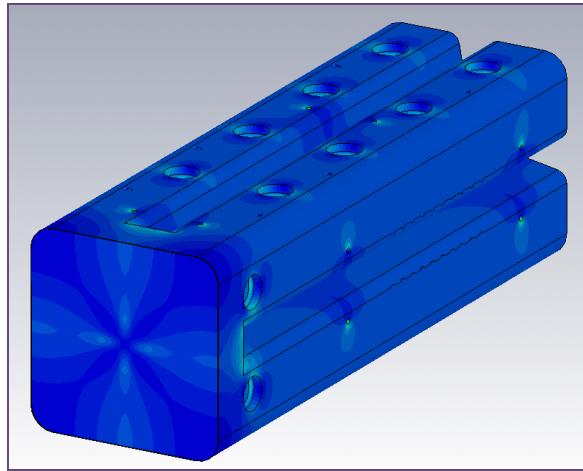
Gennady Romanov

February 4, 2013

Heating of the end-walls



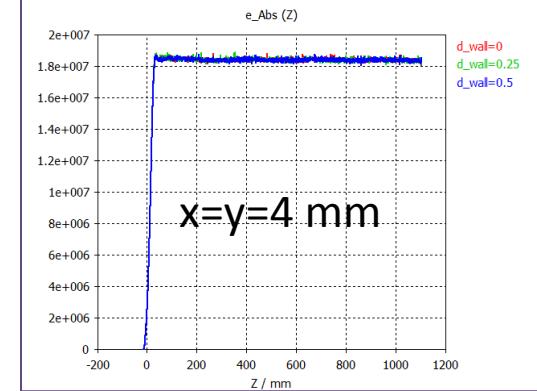
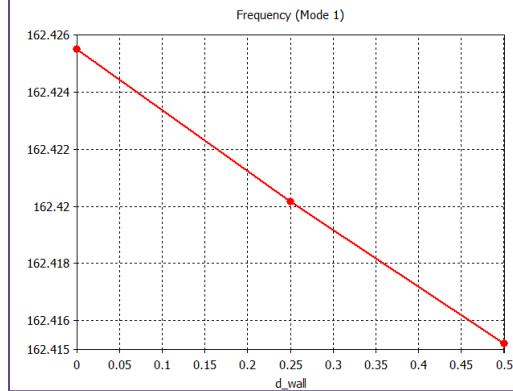
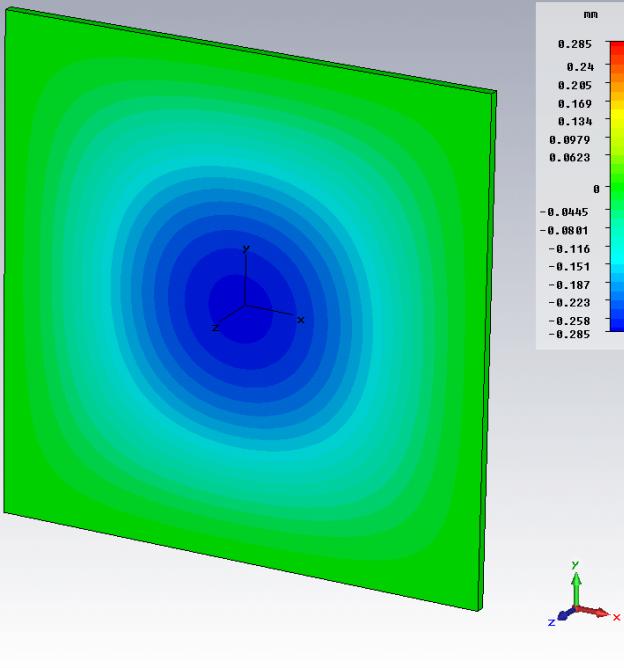
Copper plate end-wall in
the RFQ RF model



Density of the surface RF losses (logarithmic scale)

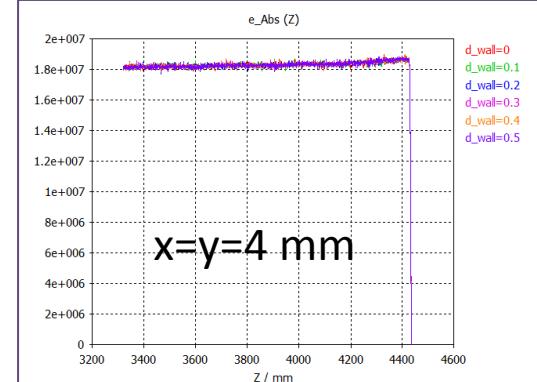
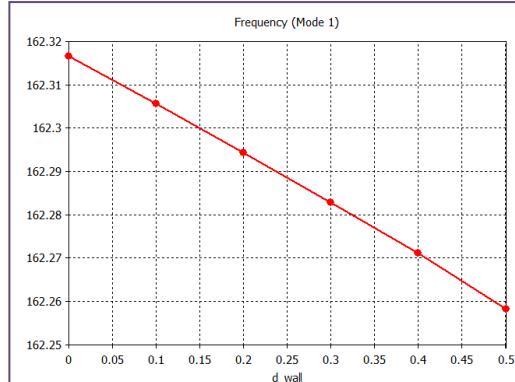
DC power losses (heat)
Input end-wall – 246 W
Output end-wall – 360 W

Deformation of the end-walls



Frequency and field distribution vs input end-wall displacement.

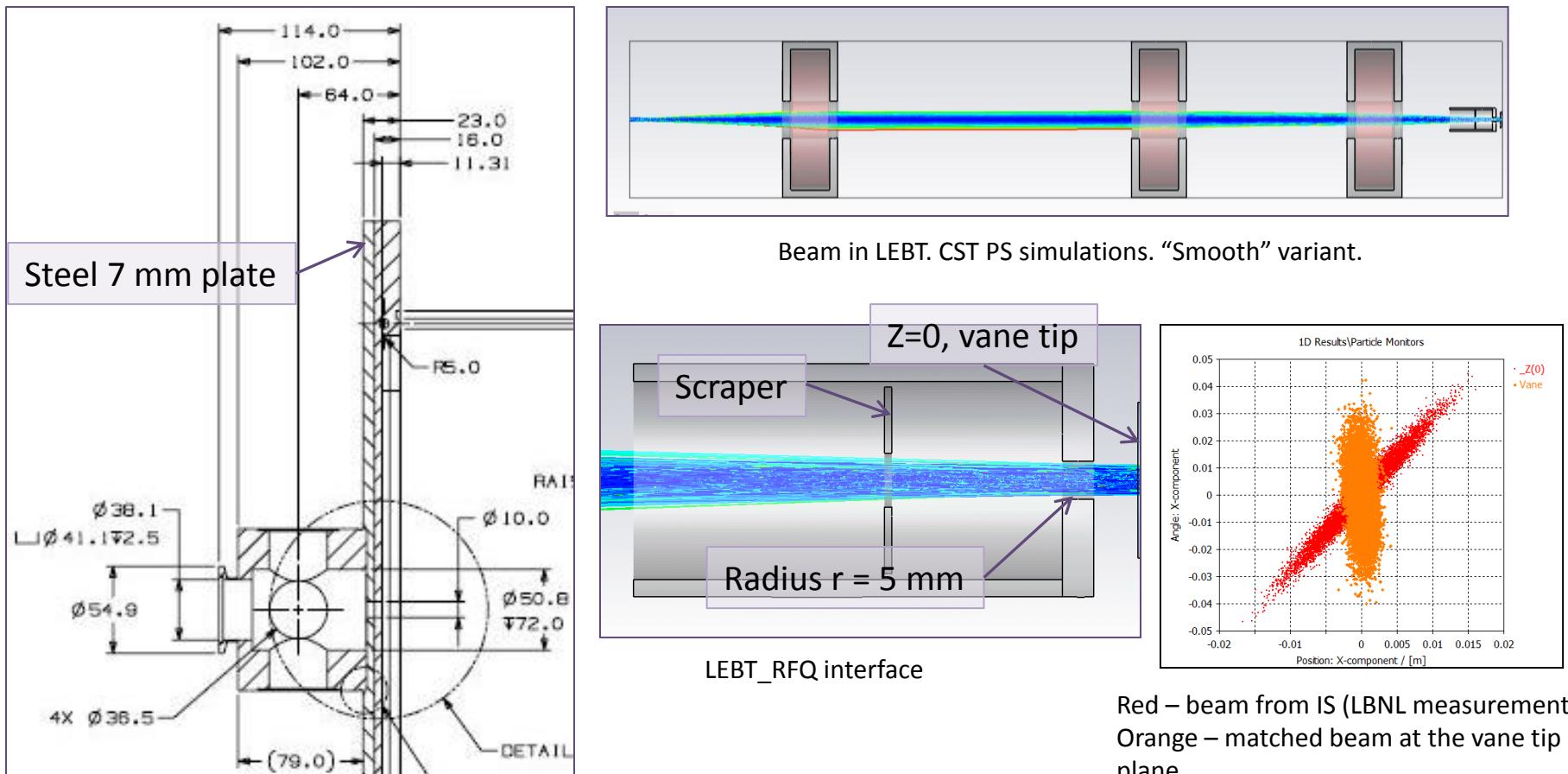
End-wall displacement due to atmospheric pressure.
Maximum displacement is 0.3 mm for end-wall enforced with steel plate 7 mm thick
(see next slide)



Frequency and field distribution vs output end-wall displacement.

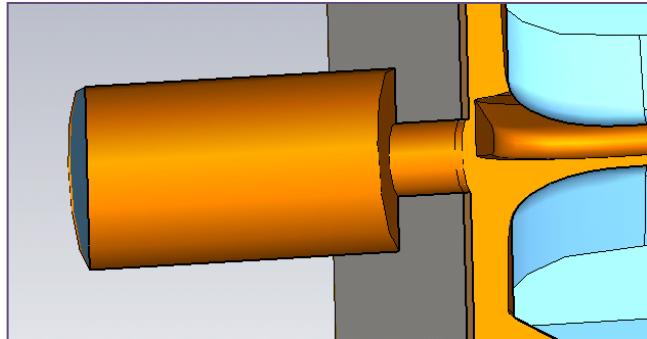
Steel plates 6-8 mm thick seems to be OK for end-plates enforcement .

Matched input beam

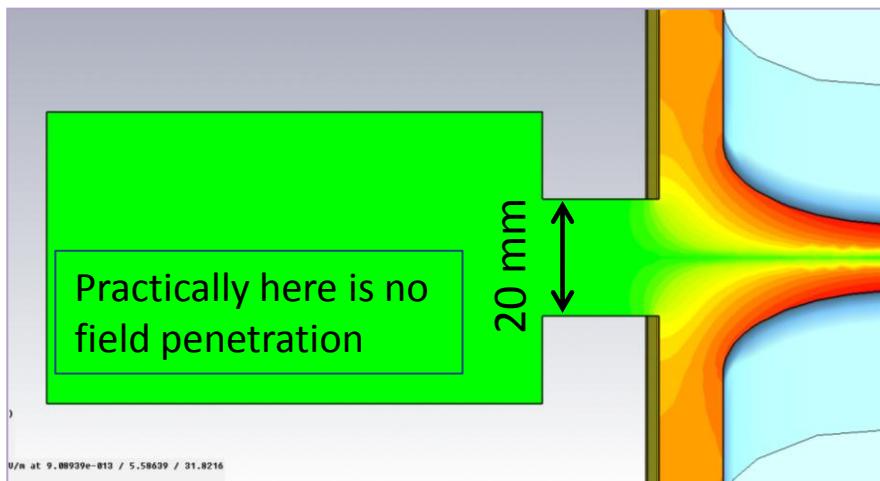


Beam matching is possible without losses, but margins are too tight.
Increase of radius r is highly desirable.

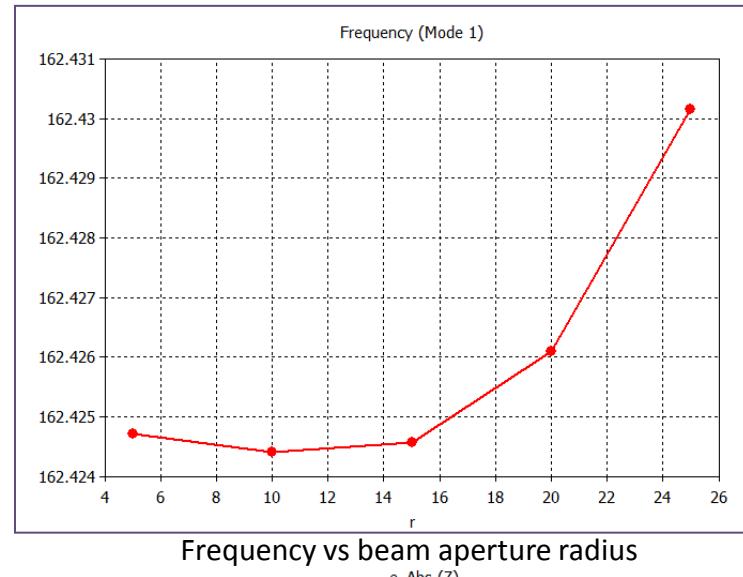
Increased input beam aperture



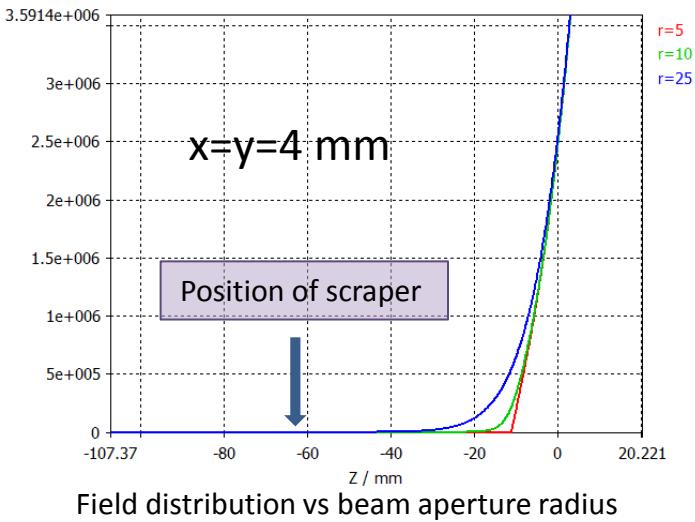
RF model of LEBT-RFQ interface



E field distribution. Logarithmic scale.



Frequency vs beam aperture radius
 $e_{\text{Abs}}(Z)$



Field distribution vs beam aperture radius

Short summary

- Generally low fields at the end-walls of RFQs provide relatively low RF losses on the walls and low sensitivity to the mechanical details in the area.
- RF losses are 246 W in the input end-wall and 360 W in the output end-wall (higher because it's closer to the vanes and surface fields are higher)
- End-wall deformations due to the atmospheric pressure cause small frequency shift and absolutely no field distortion (nice feature for fine frequency tuning). For 30 kHz frequency shift limit a steel plate of 5-6 mm would be OK to enforce input end-wall, and 7-8 mm would be OK for output end-wall
- Input beam aperture diameter can be increased up to 50 mm with negligible frequency shift of 10 kHz. Practically there is no field penetration through the beam aperture.