

# RF Modeling of the Helical Kicker for Project X

Mohamed Hassan, Timergali  
Khabiboulline, and Greg Saewert

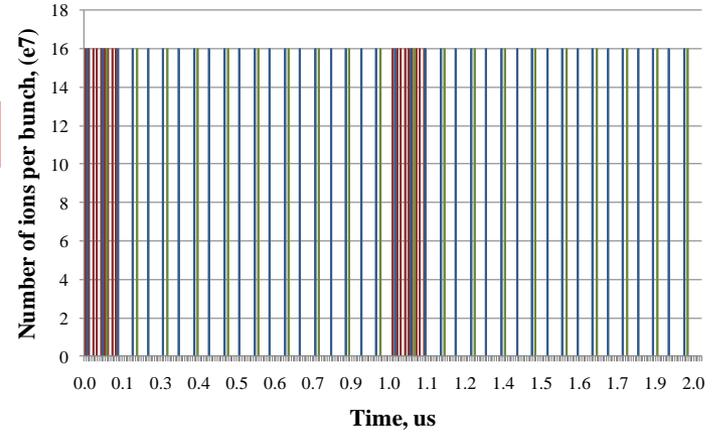
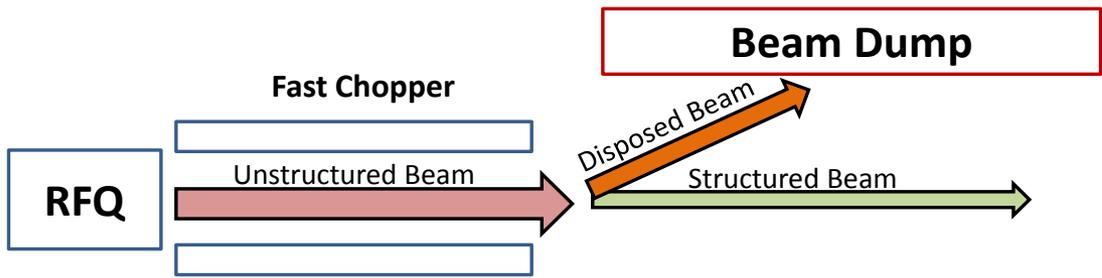
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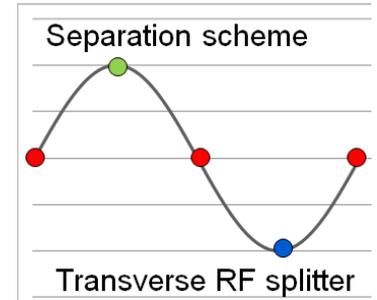
# Project X Bunch Structure

Multiple experimental program necessitates complicated bunch structures

	Train Frequency	Pulse Width (nanoseconds)
Kaon experiments	20-30 MHz	<0.2
Muon conversion experiment	0.5-1.0 MHz	<100
$\mu \rightarrow e\gamma$ & $\mu \rightarrow eee$ experiments	80-300 MHz	<0.2

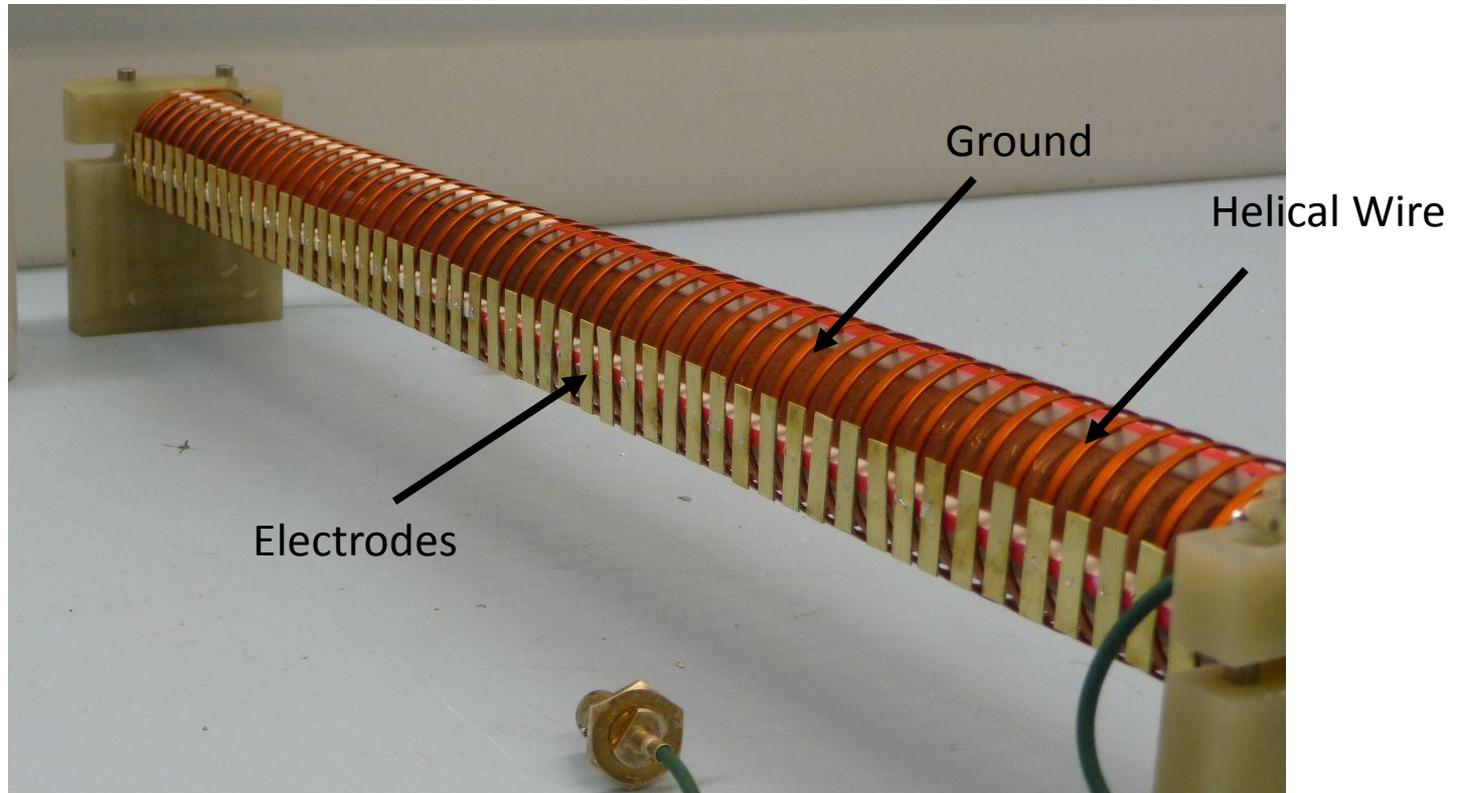


The fast chopper is needed to construct the structured bunch stream





# Helical Chopper Prototype



# Characteristic Impedance of Comparable Planar Lines

Impedance Calculation

Select Type

- Coax
- Strip Line
- Thick Strip Line
- Thin Microstrip
- Thick Microstrip
- Coplanar Waveguide w/t ground
- Coplanar Waveguide
- Thick Coplanar Waveguide
- Differential Stripline
- Suspended Microstrip
- Inverted Suspended Microstrip

permutivity: eps 1

Impedance static:  $Z_0 = 136.65$  Ohm

eps\_eff = 1.00

Geometry Data

h 0.189 W 0.105

t 0.042

Units: in MHz

Calculate Cancel Help

Phase Delay and Line Length

Frequency: 500 Linelength: 0 Phaseshift: 0

Micorstrip Line  
 $Z_0=137\Omega$

Impedance Calculation

Select Type

- Coax
- Strip Line
- Thick Strip Line
- Thin Microstrip
- Thick Microstrip
- Coplanar Waveguide w/t ground
- Coplanar Waveguide
- Thick Coplanar Waveguide
- Differential Stripline
- Suspended Microstrip
- Inverted Suspended Microstrip

permutivity: eps 1

Impedance static:  $Z_0 = 153.85$  Ohm

eps\_eff = 1.00

Geometry Data

h 0.189 W 0.105

g 0.228

Units: in MHz

Calculate Cancel Help

Phase Delay and Line Length

Frequency: 500 Linelength: 0 Phaseshift: 0

Coplanar WG  
 $Z_0=154\Omega$

Impedance Calculation

Select Type

- Coax
- Strip Line
- Thick Strip Line
- Thin Microstrip
- Thick Microstrip
- Coplanar Waveguide w/t ground
- Coplanar Waveguide
- Thick Coplanar Waveguide
- Differential Stripline
- Suspended Microstrip
- Inverted Suspended Microstrip

permutivity: eps 1

Impedance static:  $Z_0 = 201.13$  Ohm

eps\_eff = 1.00

Geometry Data

W 0.105 h 0.42

t 0.042 s 0.228

Units: in MHz

Calculate Cancel Help

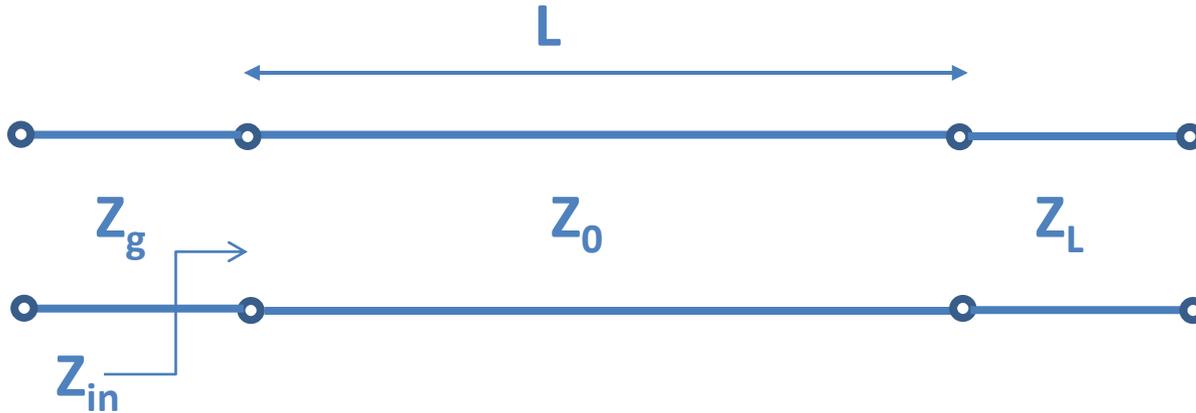
Phase Delay and Line Length

Frequency: 500 Linelength: 0 Phaseshift: 0

Differential Line  
 $Z_0=201\Omega$



# Ideal Transmission Line Model



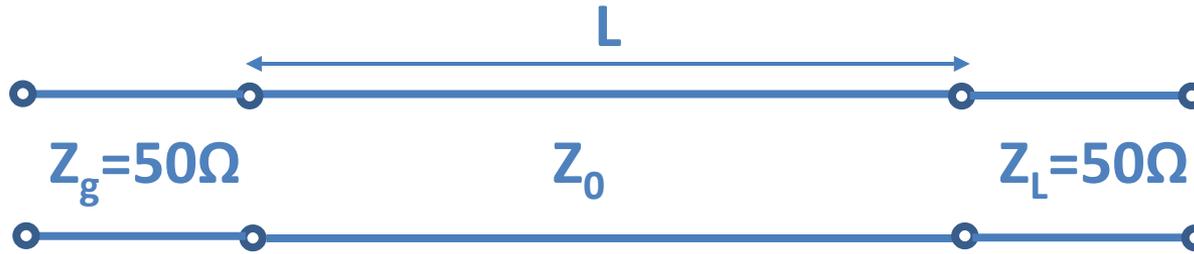
$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \cdot \tan(\beta \cdot L)}{Z_0 + jZ_L \cdot \tan(\beta \cdot L)}$$

$$\Gamma = \frac{Z_{in} - Z_g}{Z_{in} + Z_g}$$

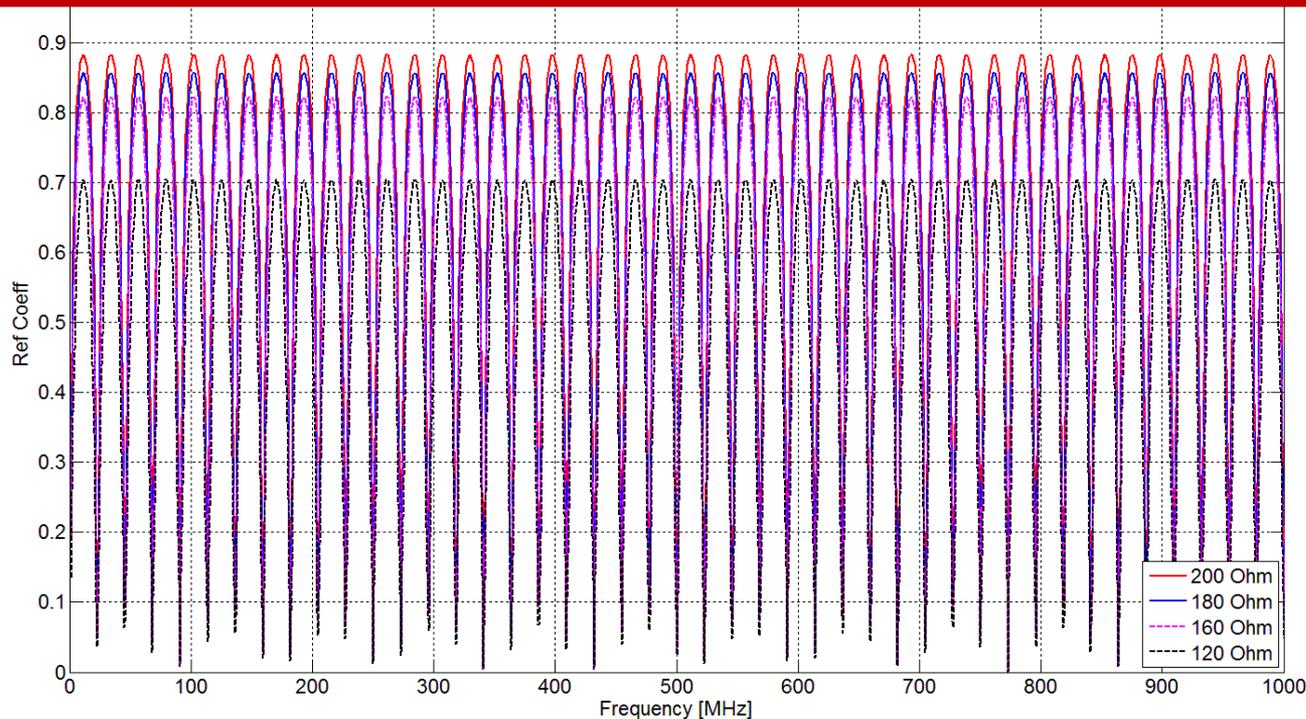
Assume  $Z_g = Z_L = 50 \Omega$  to mimic the measurement setup and vary  $Z_0$  to have a feeling about what should we expect for the reflection from the helix (if it has uniform characteristic impedance)

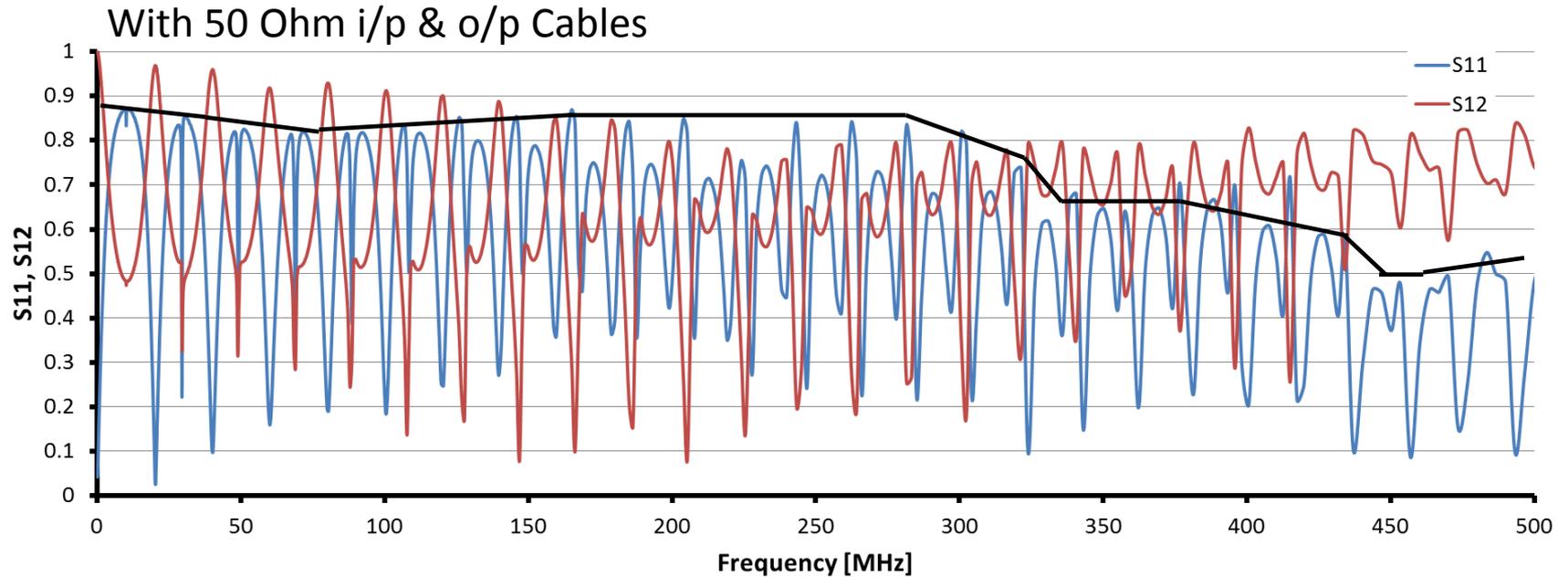


# Theoretical Reflection Response for an Ideal Transmission Line



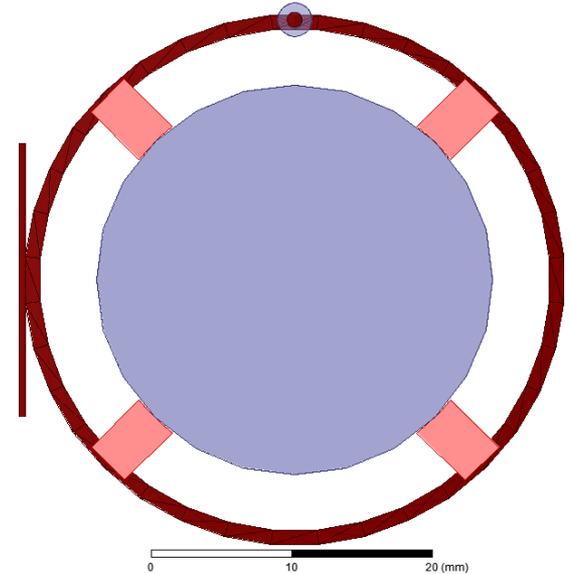
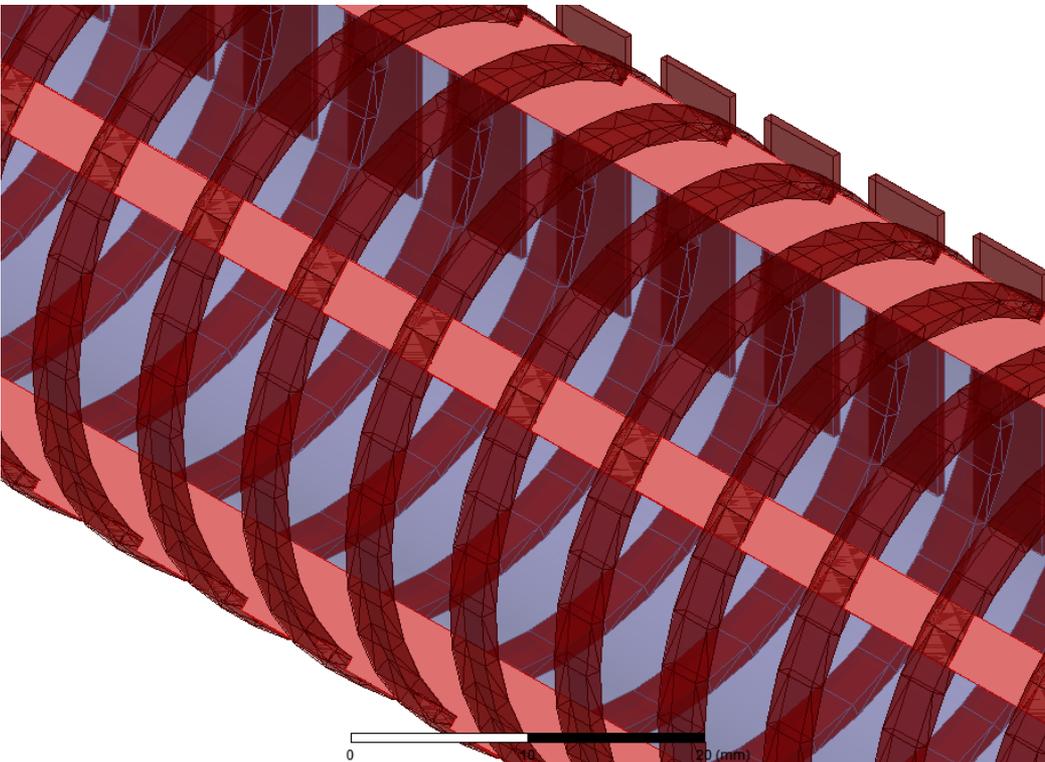
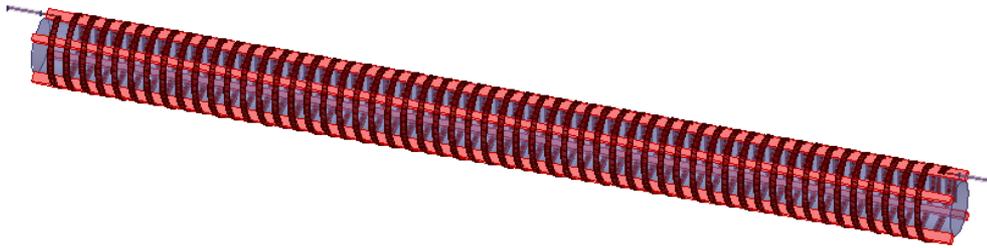
For ideal transmission line with 200  $\Omega$ , we expect about 0.88 reflection coeff.





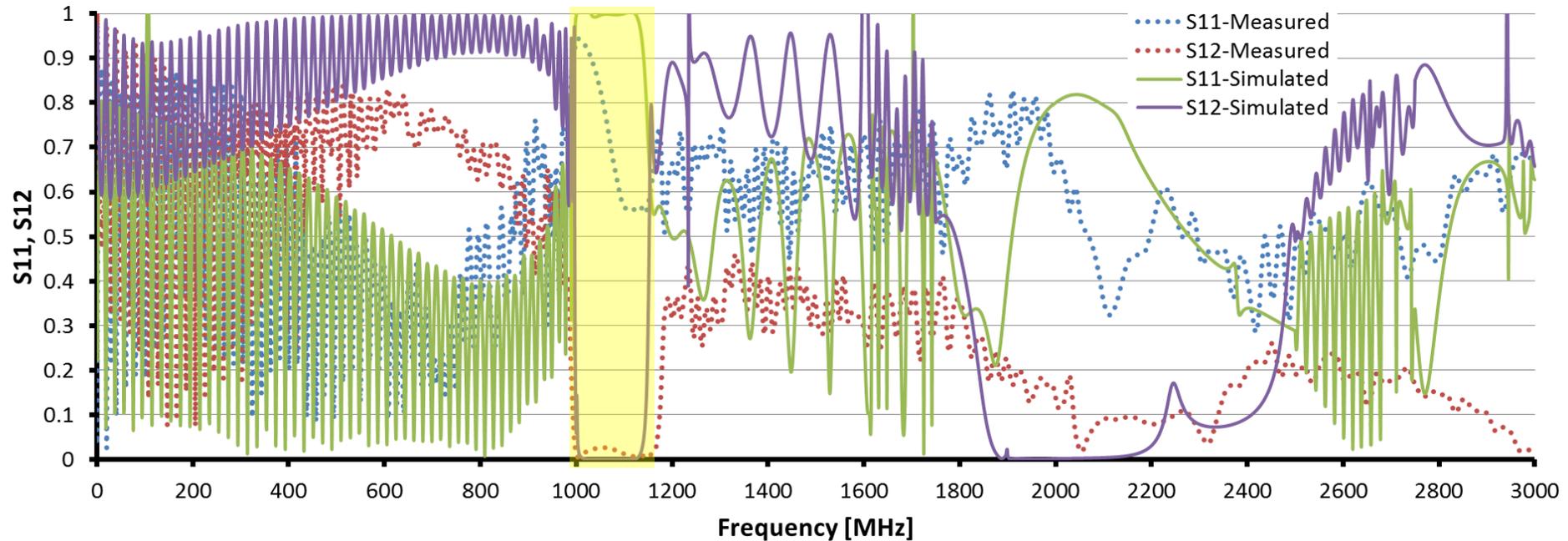
The characteristic impedance of the structure starts by about  $200 \Omega$  at 20 MHz but then changes significantly with frequency  $\Rightarrow$  Dispersion

# HFSS Model

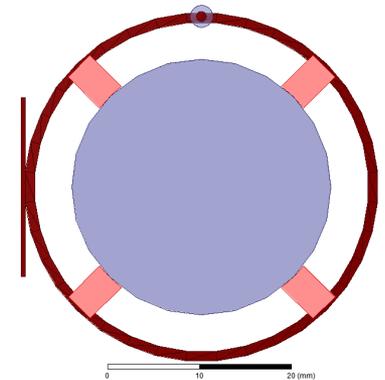


- 55 Turns
- With Electrodes
- Open to Air Except the Mirror Plane
- 50 Ohm Excitation

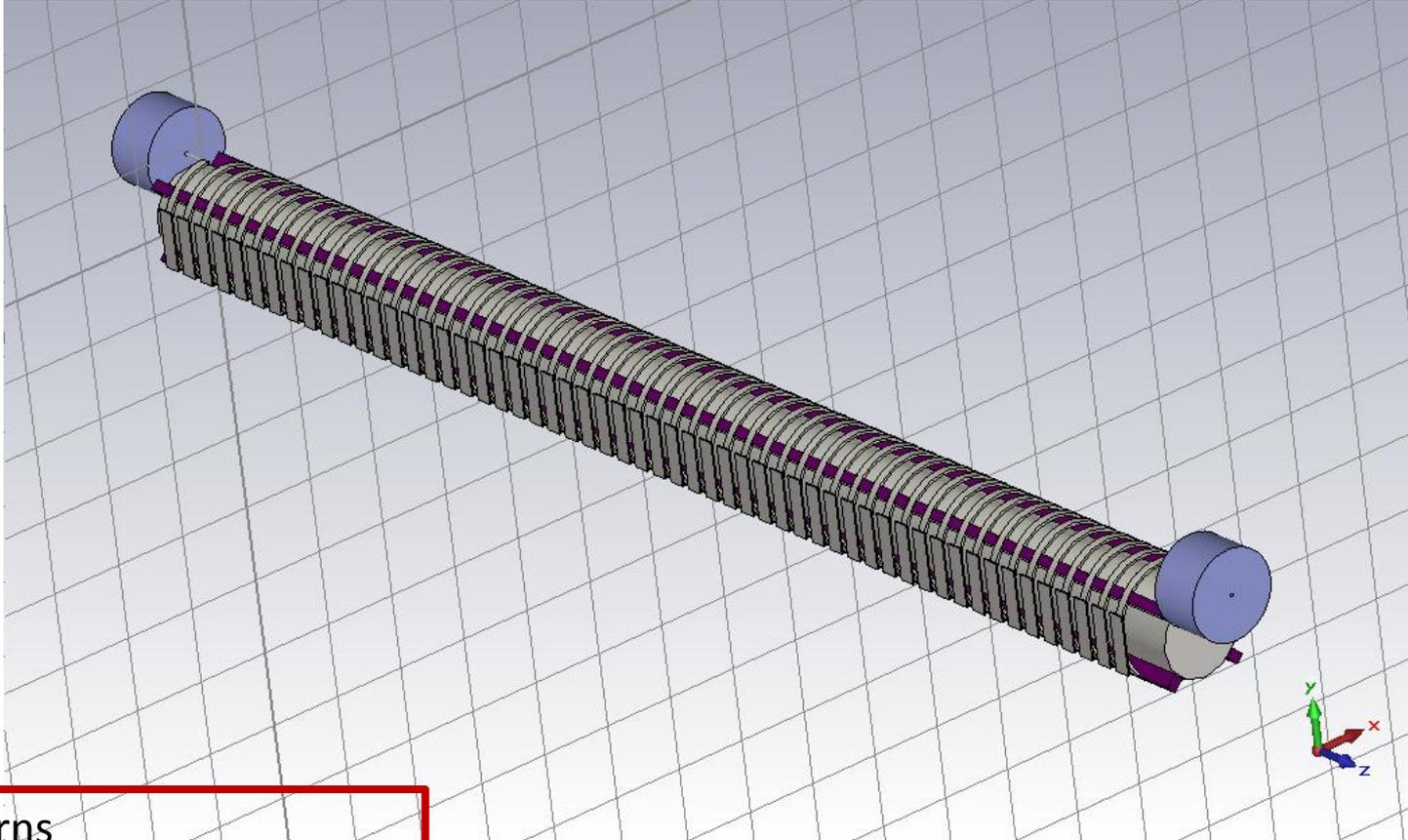
# Simulated versus Measured S-Parameters



- Periodicity of the dielectric supports causes the stop bands at 1 GHz, 2 GHz
- Simulated frequency response agrees with the measured one in terms of these stop bands of the periodic structure



# CST Model

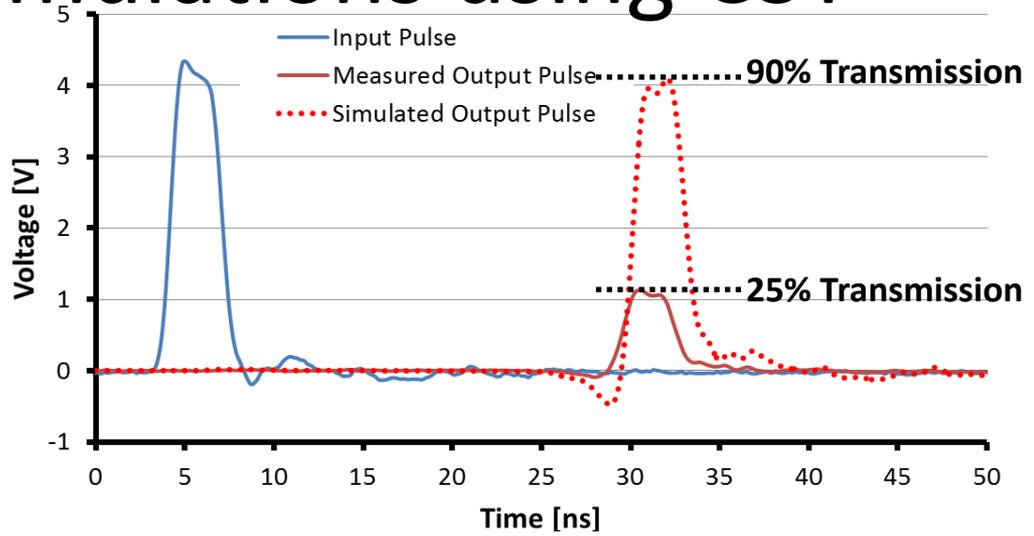


- 55 Turns
- With Electrodes
- Open to Air Except the Mirror Plane
- 200 Ohm Excitation

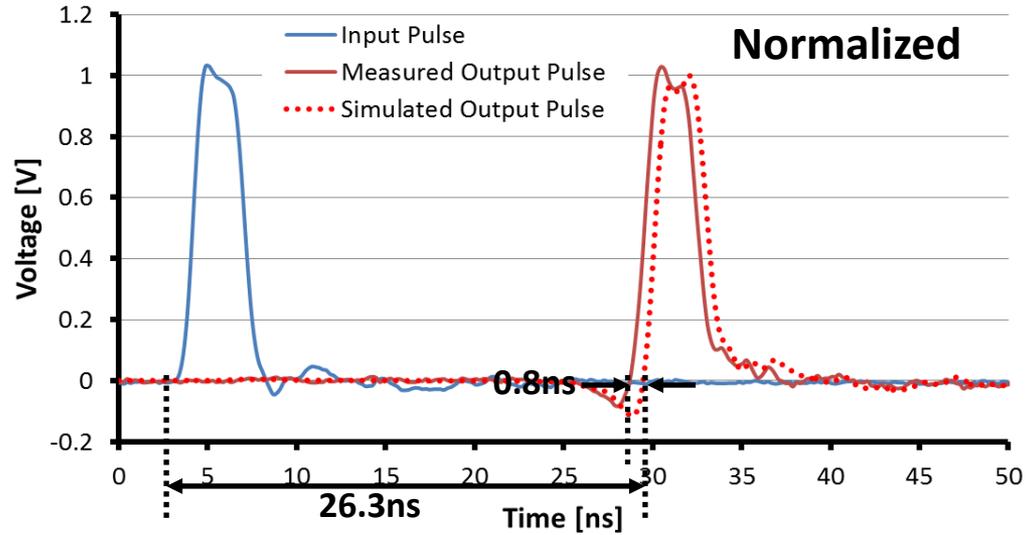


# Time Domain Simulations using CST

- Dimensions corresponds to the latest measured prototype
- Structure simulated open to air
- Actual pulse with 1ns rise\fall time was used as excitation



- Simulated pulse delay for **0.333"** pitch is 26.3 ns
- Need to account for 1" input/output coaxials  $\sim 2"/3e8 = 0.17$  ns
- Delay in the helical structure is 26.1 ns



- About 0.8 ns difference between the simulated and measured transmission pulses
- Simulation shows better transmission of the pulse through the structure
- Due to the different excitations used in simulation and measurements

# Adjusting the Delay

$E=2.1 \text{ MeV}$  --  $\text{Gamma}=E/940.85[\text{MeV}]+1$ ,  $\text{Gamma}=1.002232$ , Targeted  $\beta_g 0.0667$

$hs=0.189''$

$L=N*P$

$v=L/\text{Delay}$

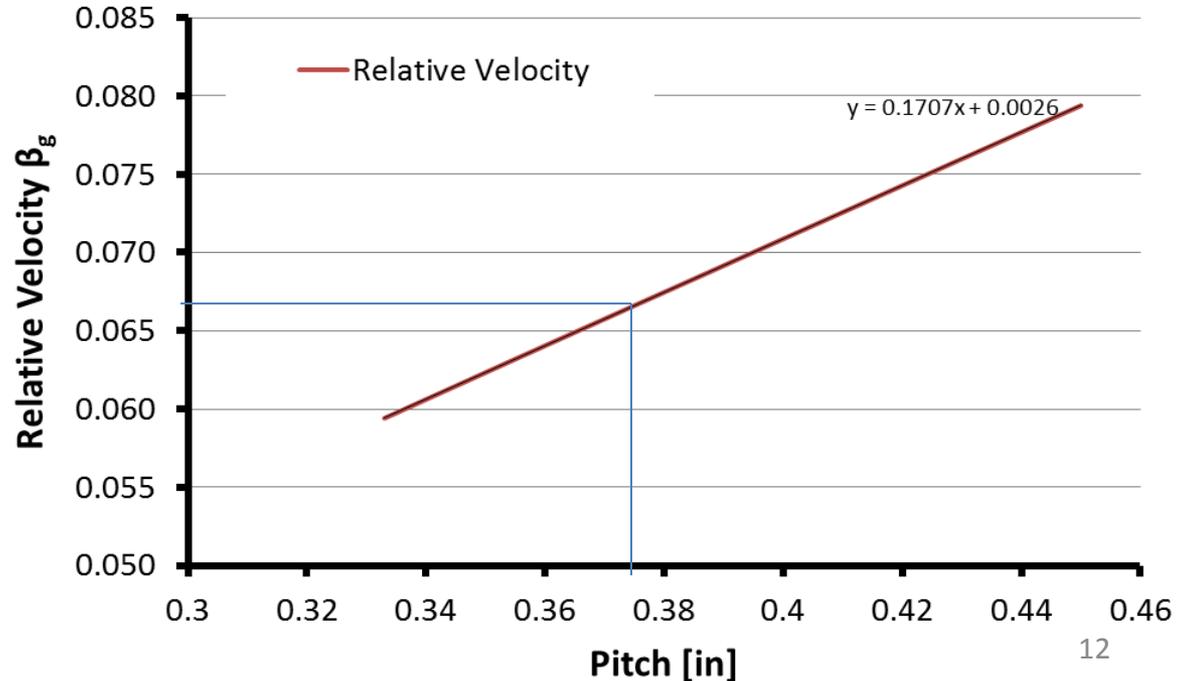
$\beta_g=v/c$

	L, Delay	$\beta_g$
$P=0.333''$	465.2 mm, 26.1 ns	0.05941
$P=0.370''$	516.89 mm, 26.2 ns	0.06576
$P=0.450''$	628.77mm, 26.4ns	0.07939

$$P = (\beta_g - 0.0026) / 0.1707$$

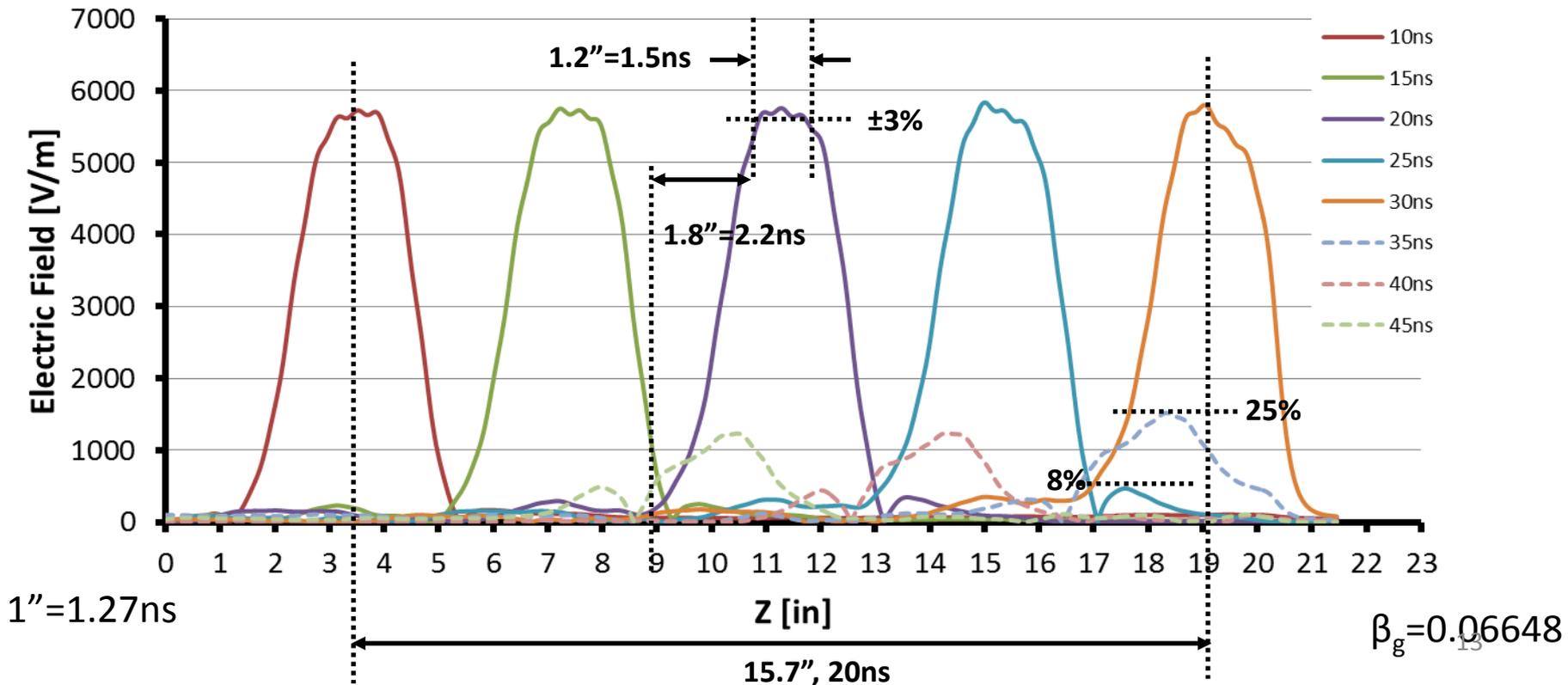
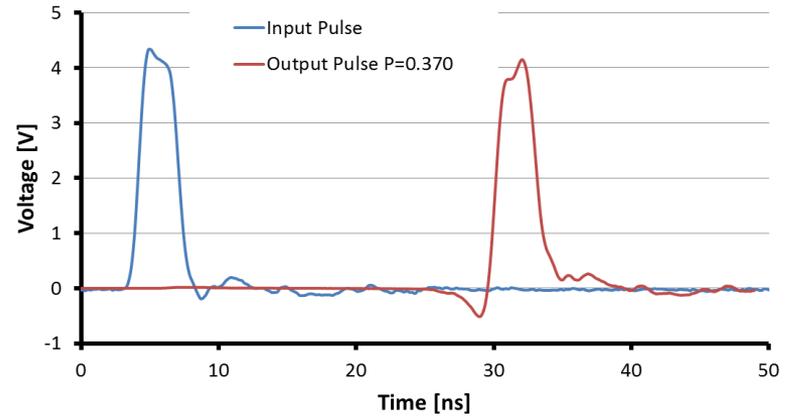
$$P = 0.376''$$

- To get the targeted value of the delay, the pitch need to be changed



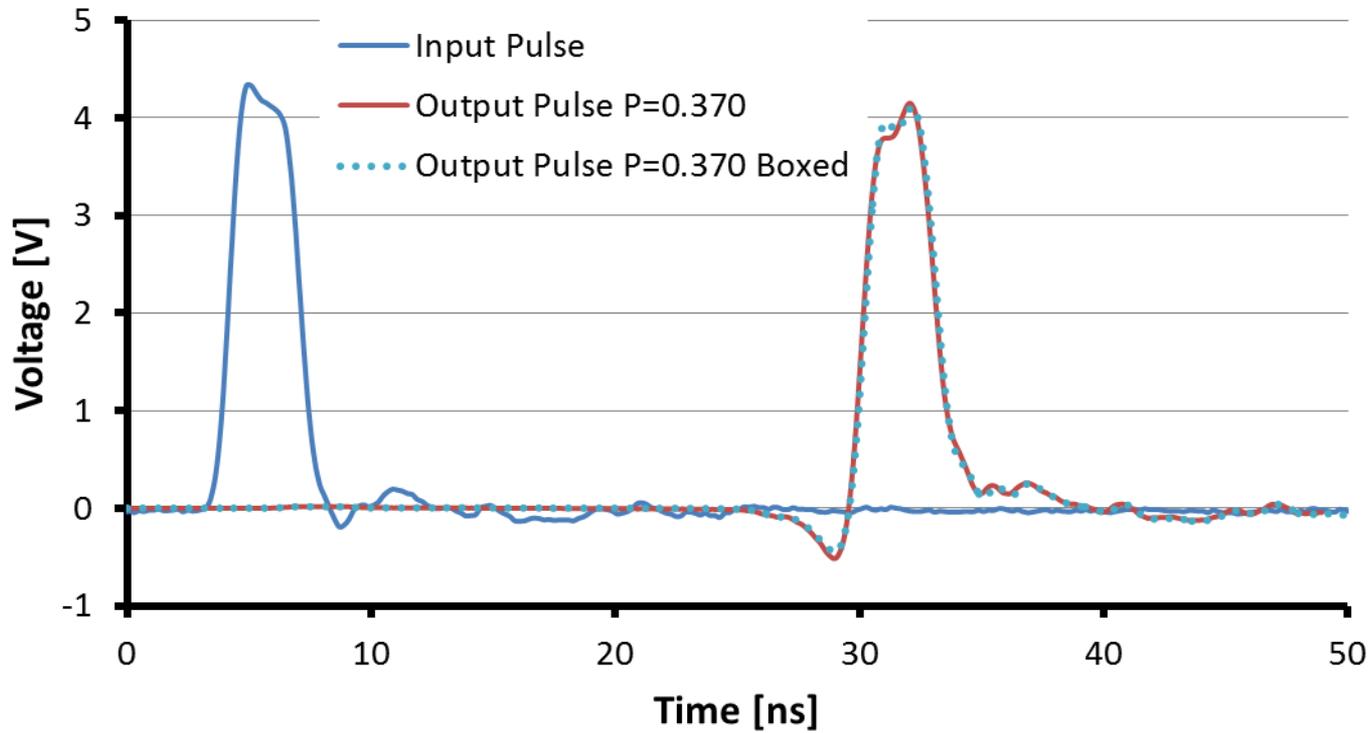
# Field on Beam Axis

- Field on beam axis for  $P=0.37''$
- Actual input pulse with 2ns hold time and 1ns rise/fall time
- 200  $\Omega$  input/output excitation to the structure



# Open vs Boxed Structure

- Used a box according to the drawing 2251

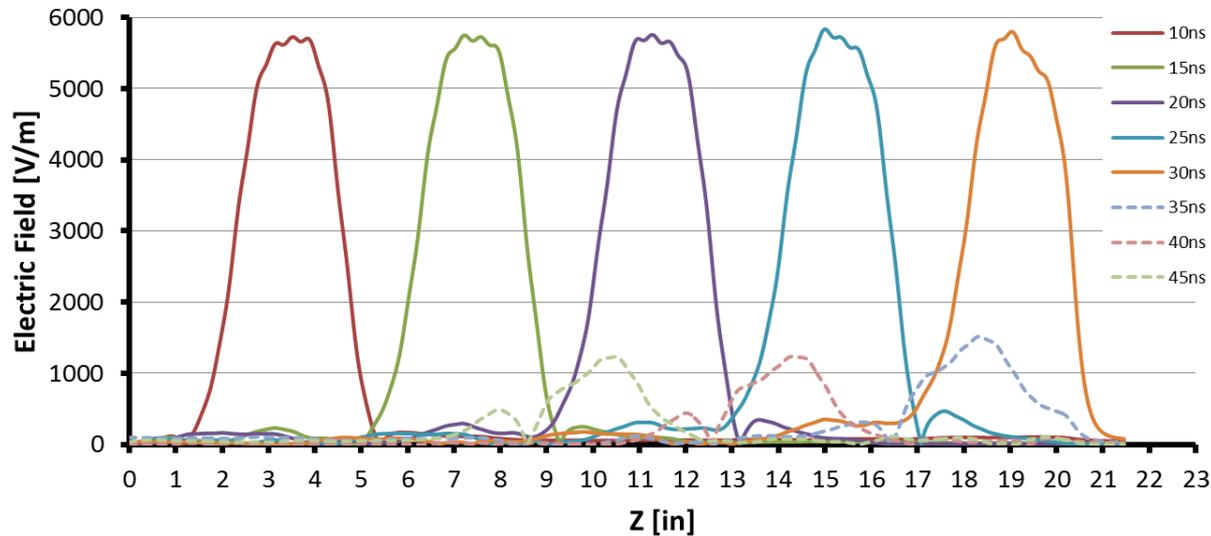


Delay didn't change upon boxing the structure

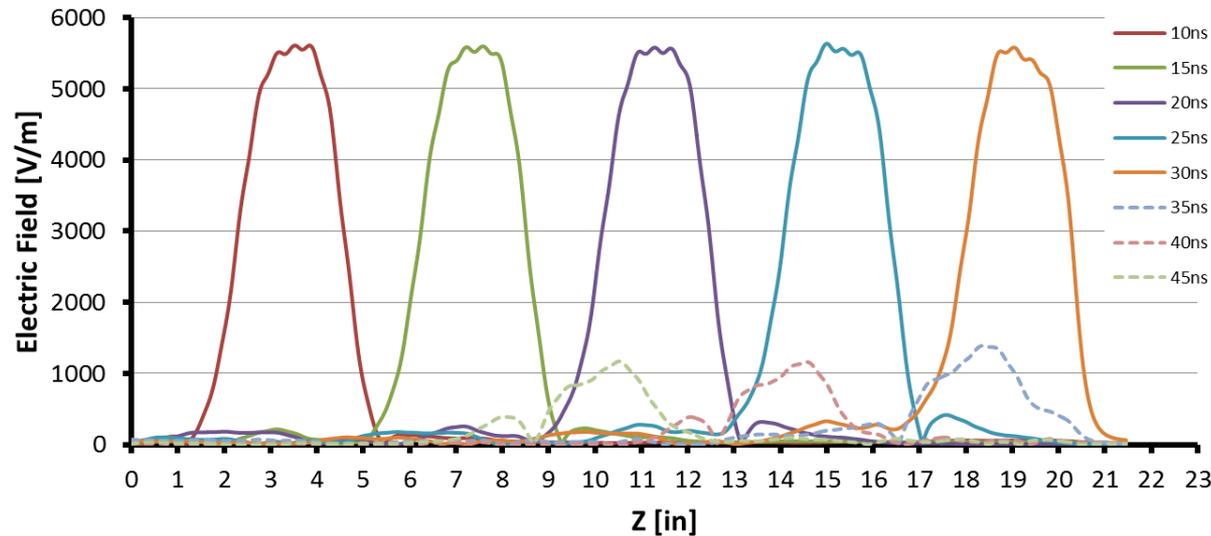


# Open vs. Boxed Structure

Open



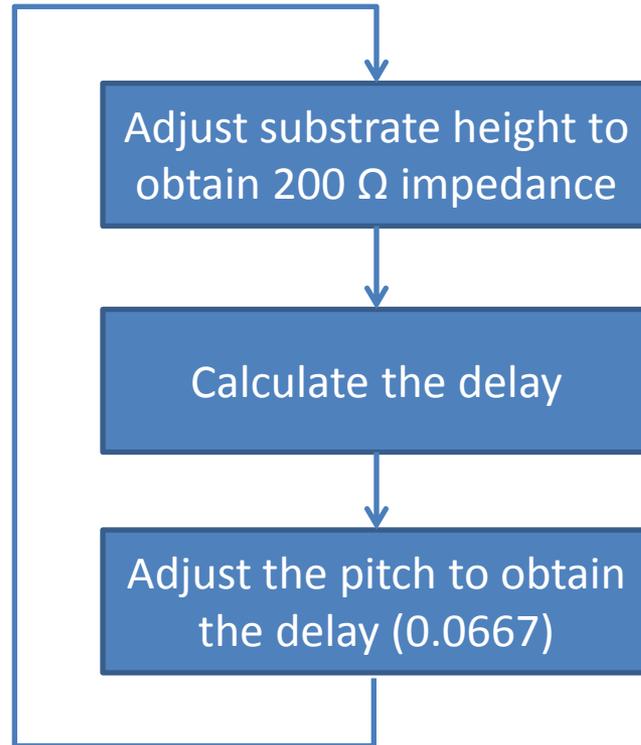
Boxed



Dispersion looks a little bit better after boxing the structure



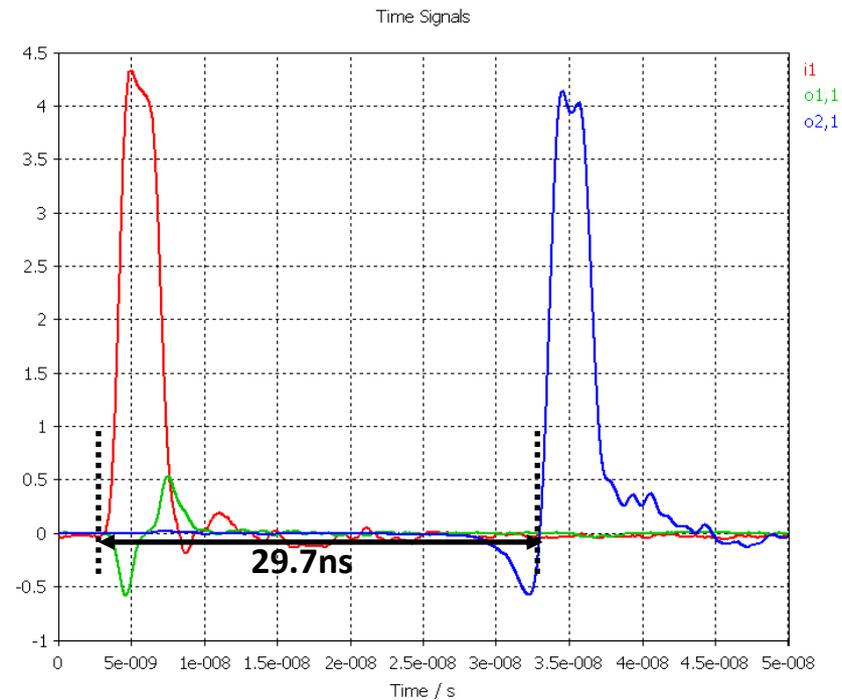
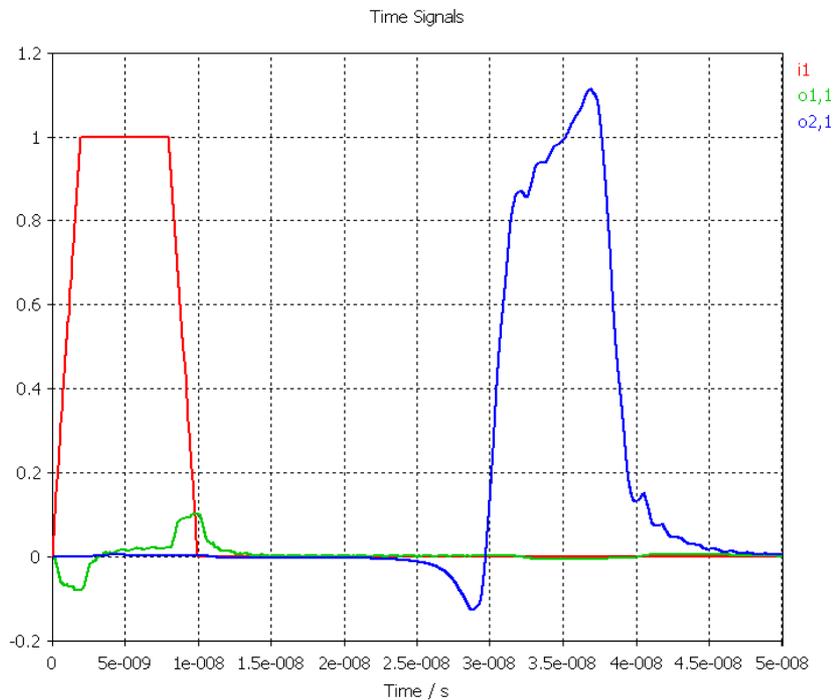
# Adjusting the impedance and delay



Getting both the impedance and the delay required few design iterations changing the substrate height and pitch

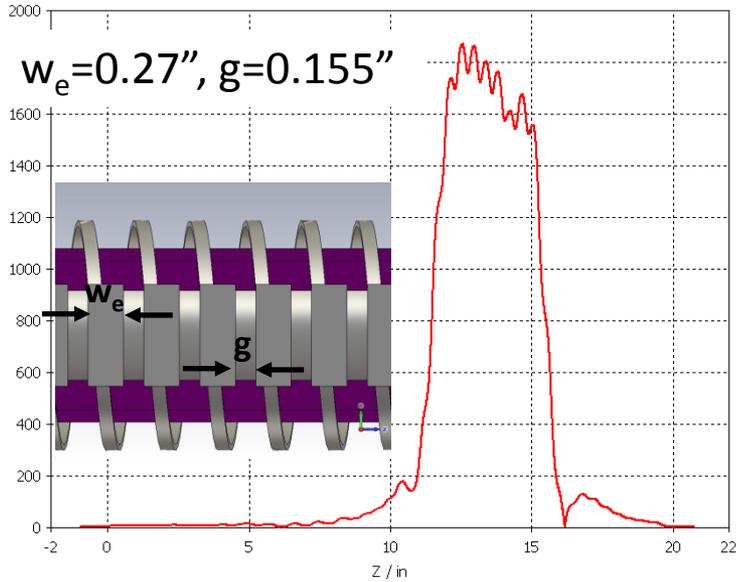
# Final Design

- Substrate height (metal to metal in different to the sketch)  $h_s=0.285''$ ,  
 $h=h_s+t/2=0.306$
- Pitch= $0.425''$
- Everything else is the same

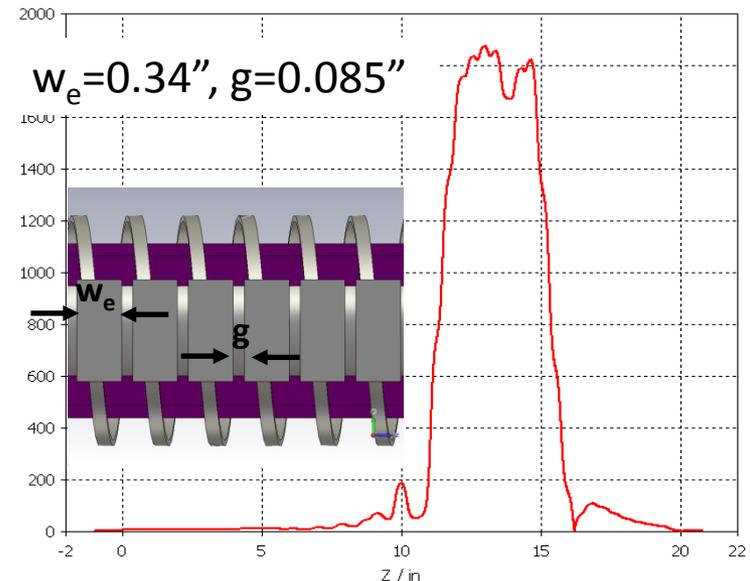
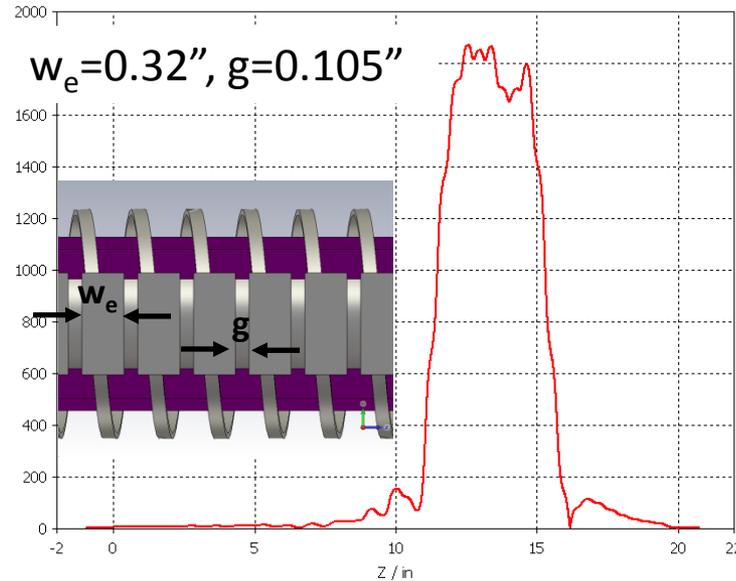
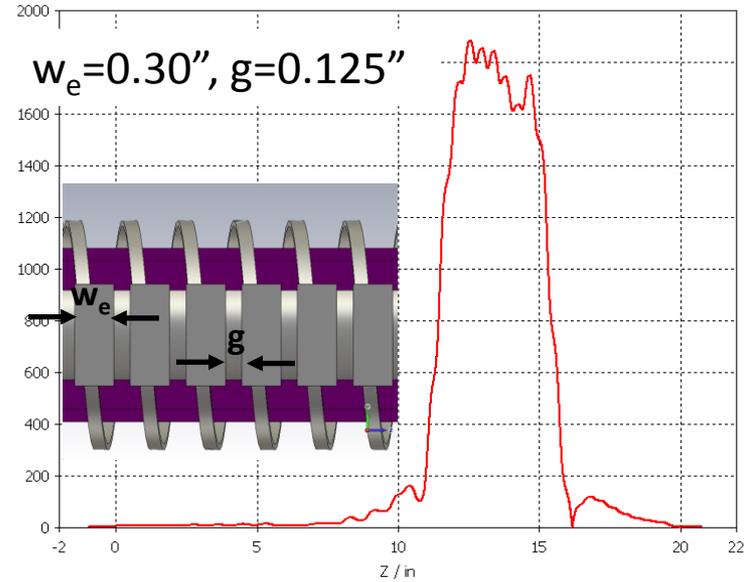


# Effect of Changing Electrode Size

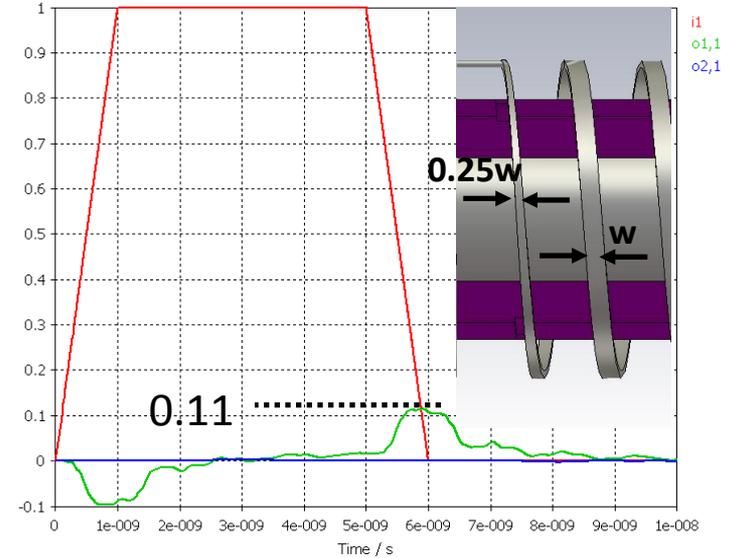
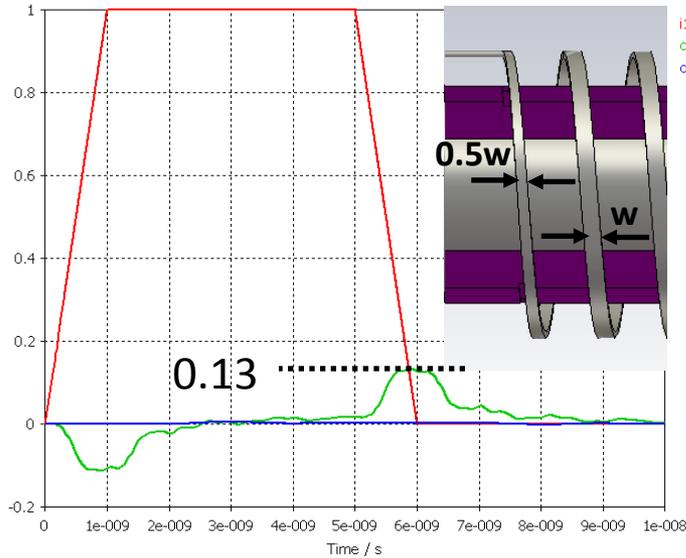
e-field (t=0.5e-8(1e-9)) (1)\_X (Z)



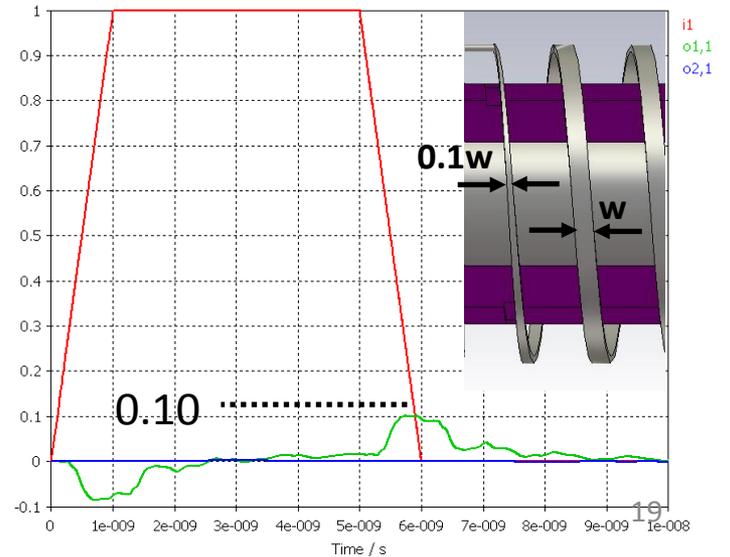
e-field (t=0.5e-8(1e-9)) (1)\_X (Z)



# Effect of Flaring the Wire Ends

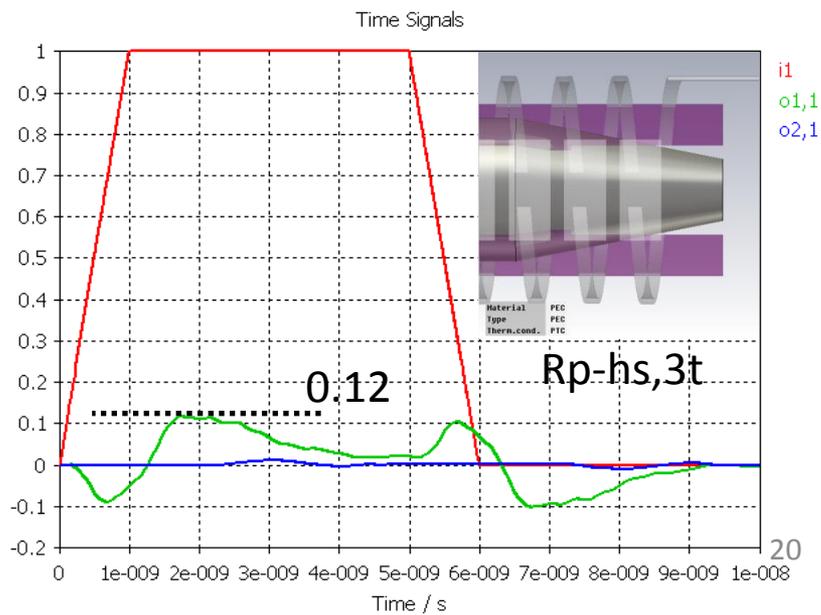
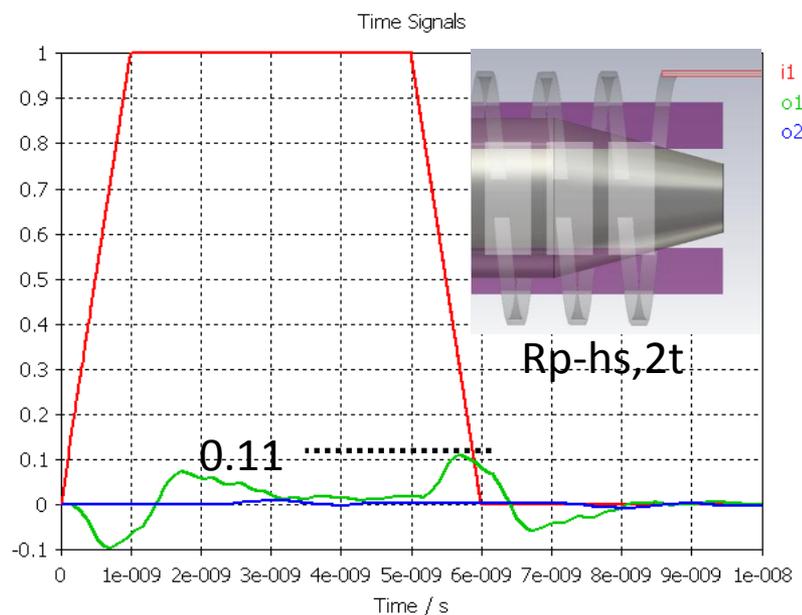
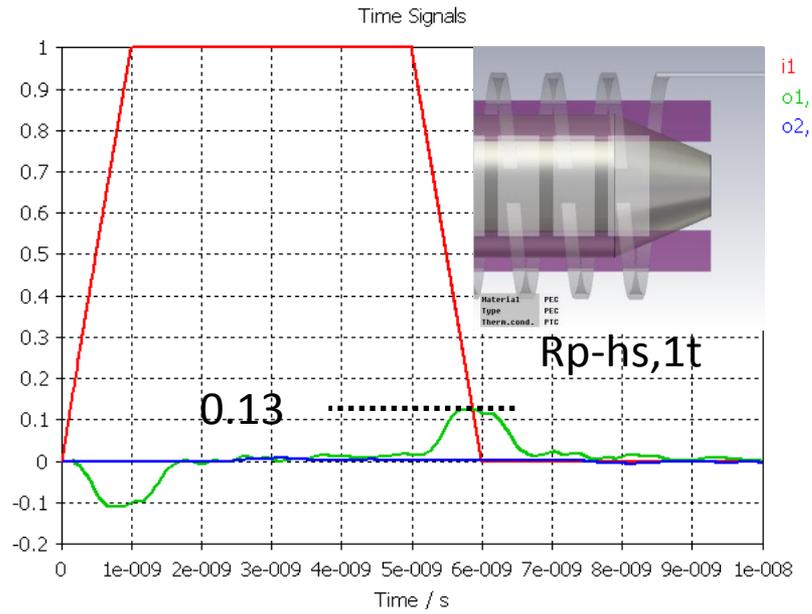
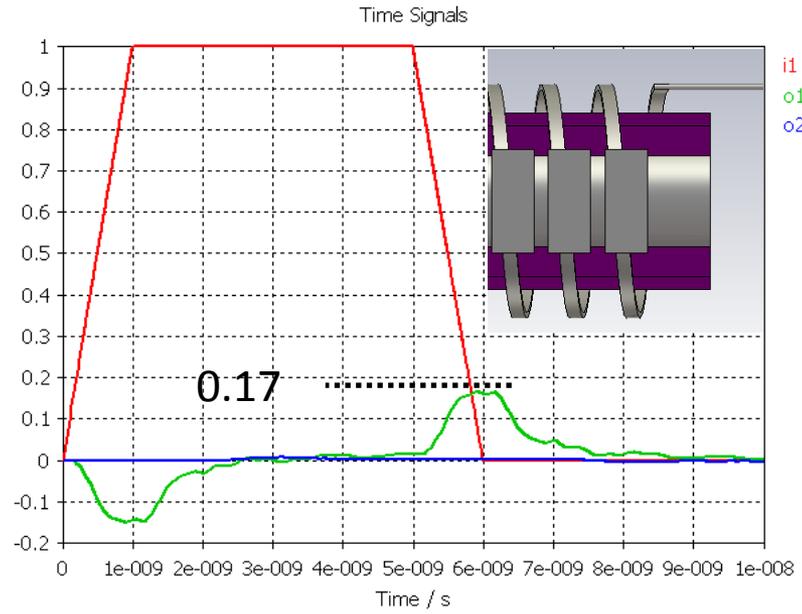


The wire would need to get too thin,  
which is unrealistic to implement

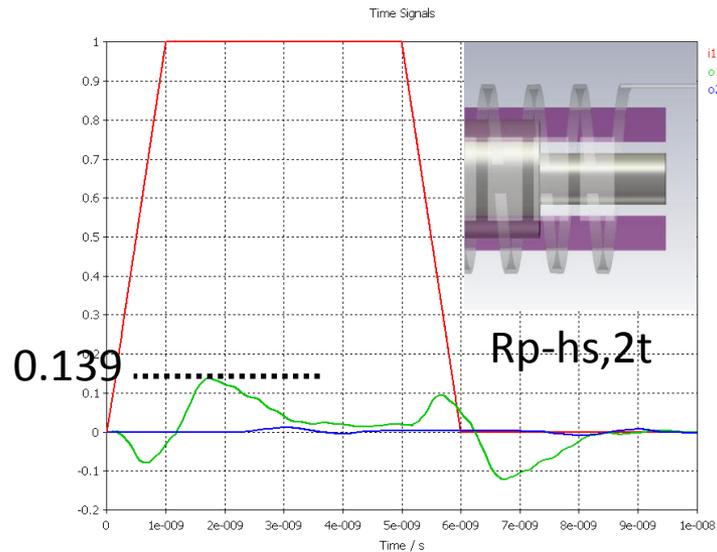
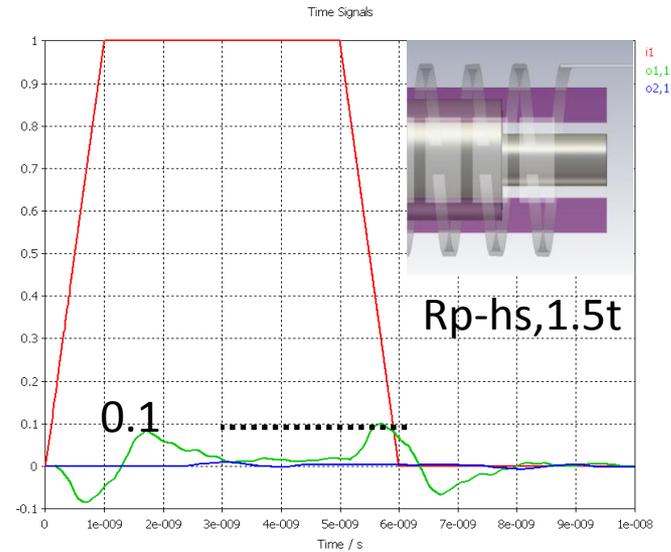
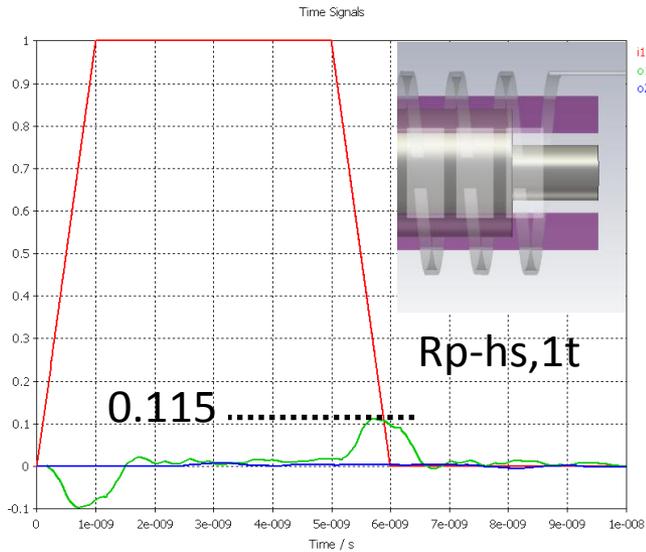




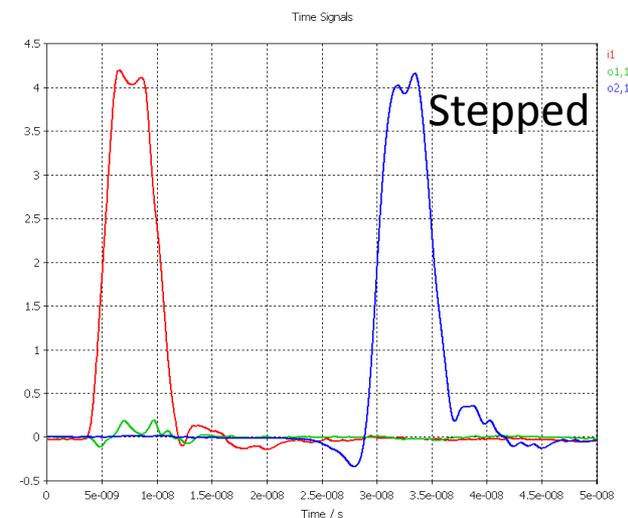
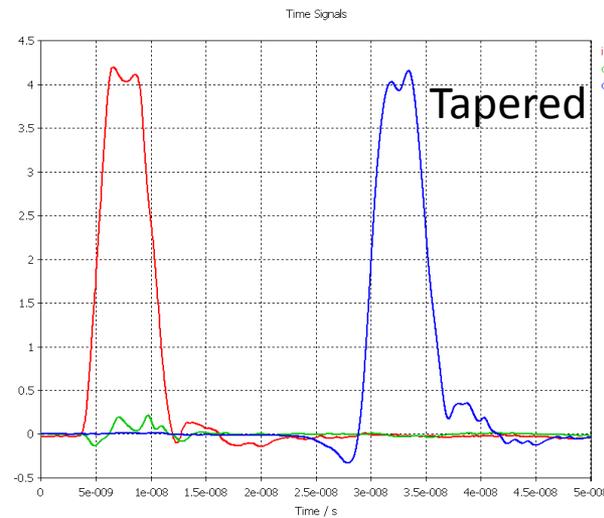
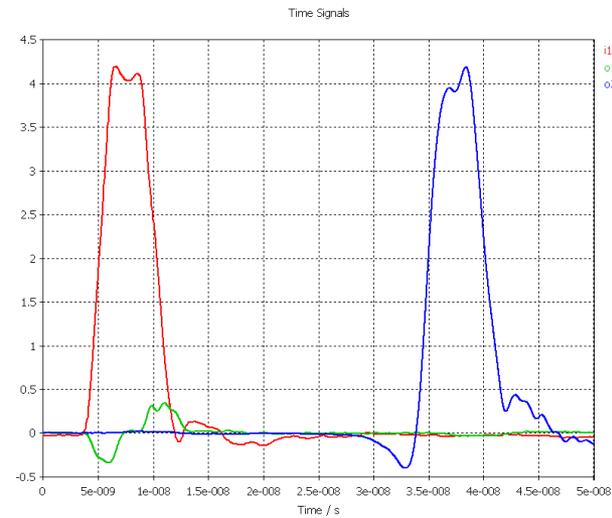
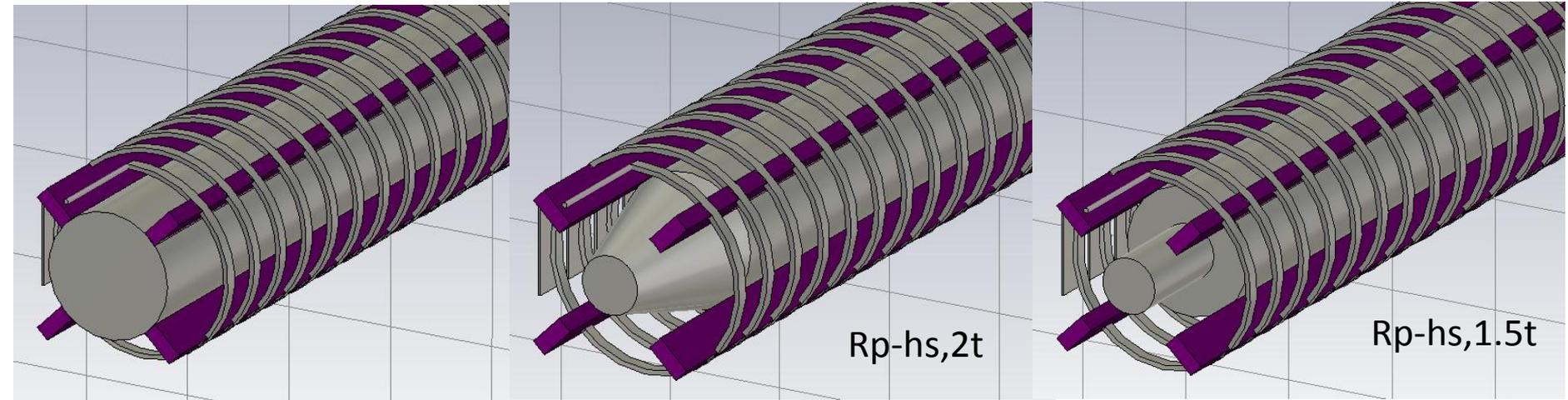
# Tapering Ground Tube



# Stepped Ground Tube



# Design with End Effects Compensation





# Conclusion

- The helical kicker has been thoroughly modeled
- Pitch of 0.425" is recommended to match the beam velocity with dielectric support of height 0.285" to get the 200  $\Omega$  impedance
- Boxing the structure with the current dimensions on drawing 2251 has negligible effects on the structure performance
- End effects could be compensated by flaring(or stepping) the ground for a couple of turns at the ends