



# RF Simulation Studies of PXIE RFQ.

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**Collaboration Meeting at LBNL**



The simulations of IMP and PXIE RFQs are performed per the LBNL's requests.  
The list of tasks:

2D simulations (RFQ cross-section):

- Frequency, Q-value, power dissipation per length unit.

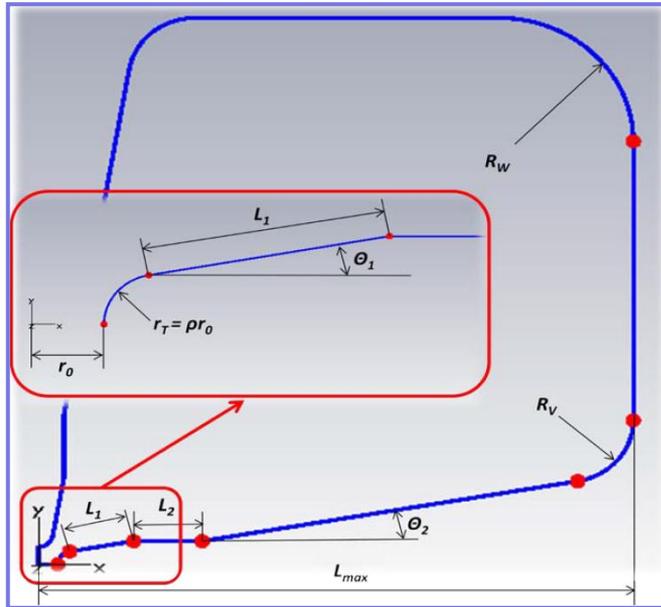
3D simulations:

- Frequency shift/perturbation from pi-rods and Q value (or power dissipation by rods);
- Frequency sensitivity from tuners, and frequency shift/perturbation from tuners at their nominal intrusion and power dissipation by the tuners;
- Perturbations to field distributions due to pi-rods and tuners;
- Frequencies of dipole modes with and without pi-rods;
- Cut-back designs to provide flat field flatness and frequency of 162.5 MHz;
- Power dissipation (and density) at cut-backs and Q value of the whole RFQ structure with everything.

The results are updated on the permanent basis, so today the focus will be on the simulation procedures mostly.



# RFQ cross section profile



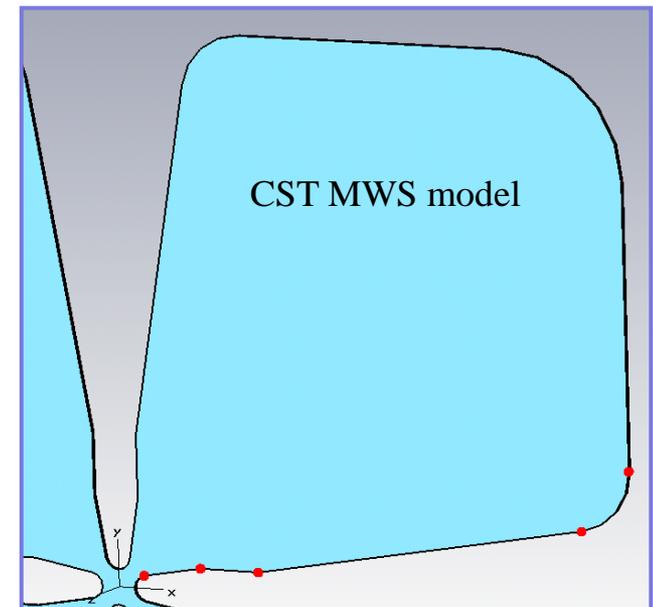
Key points	x	y
0	0	0
1	5.576	0
2	6.554402	2.688138
3	9.031803	4.118466
4	28.72796	7.59143
5	48.72796	7.59143
6	158.273	26.90717
7	170.1209	33.74757
8	174.8	46.60332

Control points from CST MWS model

X	Y
9.032e+000	4.118e+000
2.873e+001	7.591e+000
4.873e+001	7.591e+000
1.583e+002	2.691e+001
1.748e+002	4.660e+001

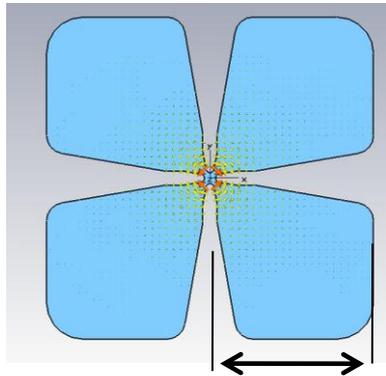
Control points from J.Staple's spreadsheet

No	Variables	PXIE	Unit	Comments
1	$r_0$	0.5576	cm	
2	$\rho$	0.75		Ratio of vane tip radius to $r_0$
3	$L_1$	2	cm	Horizontal/vertical length of the sloped lines
4	$L_2$	2	cm	Horizontal/vertical length of the straight lines
5	$\theta_1$	10	Deg.	First angle of the vane
6	$\theta_2$	10	Deg.	Second angle of the vane
7	$R_V$	2	cm	Curvature of the vane corner
8	$R_W$	4	cm	Curvature of the RFQ cavity wall
9	$L_{max}$	17.48	cm	Maximum inner cavity length
	$r_T = \rho r_0$	0.418	cm	Transverse tip radius (derived parameter)

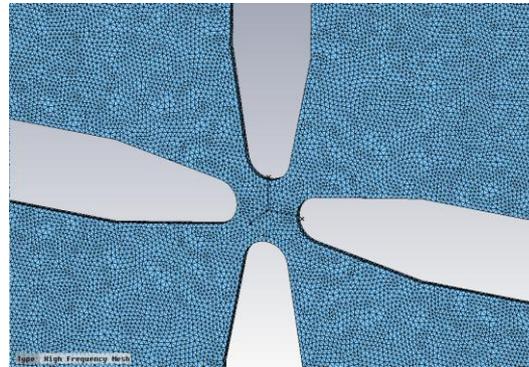




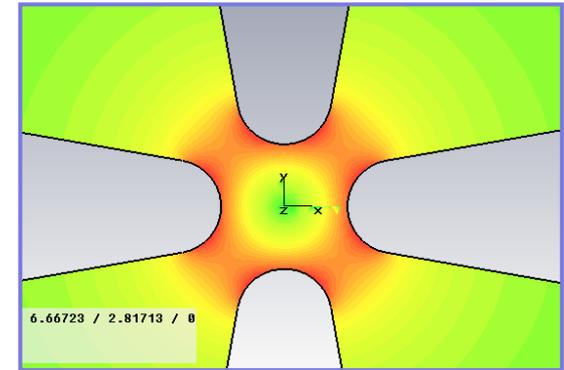
# RFQ cross section simulation



$L_{\max}$



Mesh, 495,000 tetrahedrons

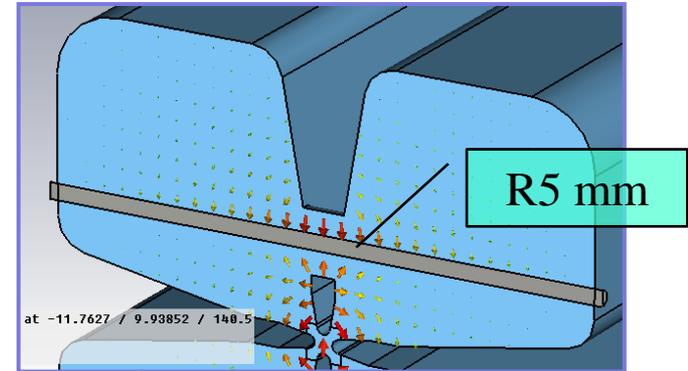
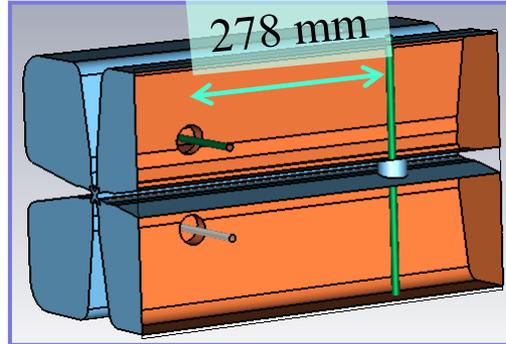
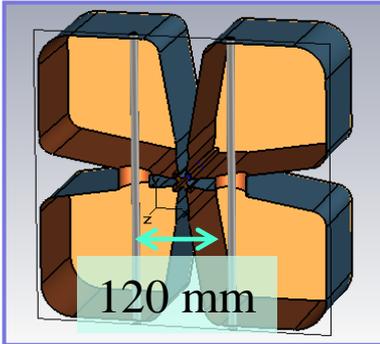


$E_{\text{abs}}$  distribution

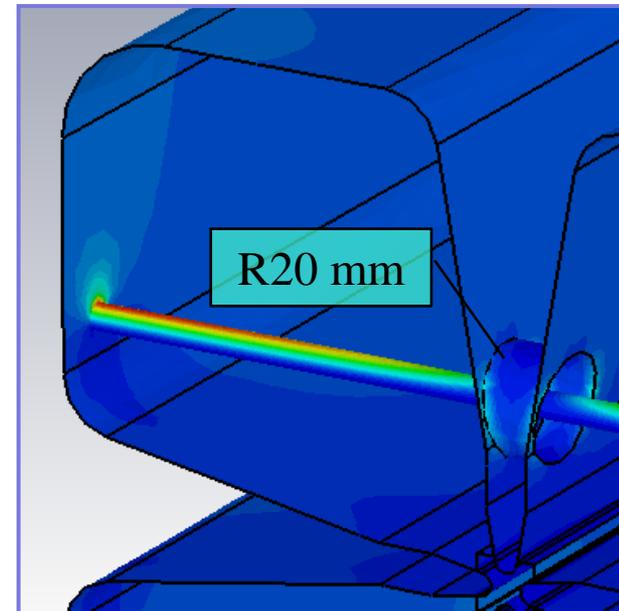
Parameters	Original	Tuned
Frequency, MHz	164.39	162.492
Q factor	16747	16813
Power loss per length, W/cm	138.89	133.0
Peak electric field, MV/m	13.4	13.4
Dipole mode freq., MHz	159.33	157.5
Tuning coef. $\Delta F/\Delta L$ , MHz/mm	1.04	1.04
$L_{\max}$ , mm	174.8	176.59



# Pi-mode rods period



E field

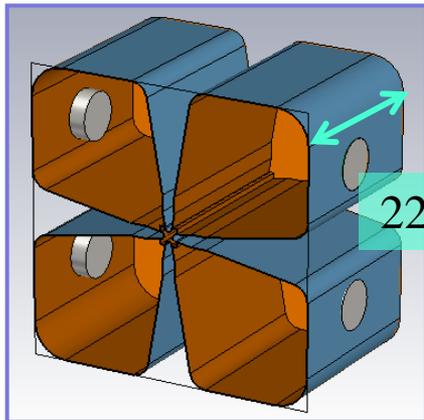


Loss density distribution

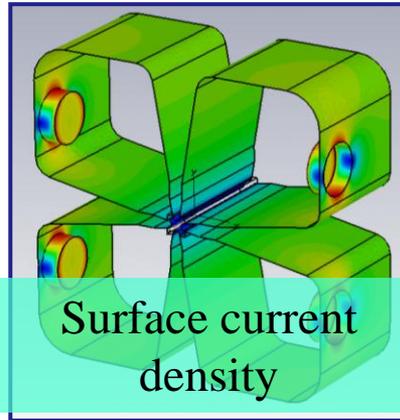
Parameters	Value
Frequency, MHz	162.486
Frequency shift due PISLs, MHz	-5.56
Q factor	15333
Q factor drop due PISLs, %	-9.65
Power loss per PISL, W	188
Dipole mode freq., MHz	179.6
Dipole mode shift., MHz	22.1
Field perturbation at x=y=5 mm, %	0.3
$L_{\max}$ , mm	171.44



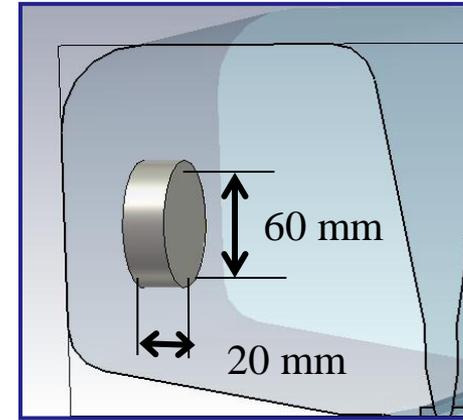
# Tuner period



222.4 mm



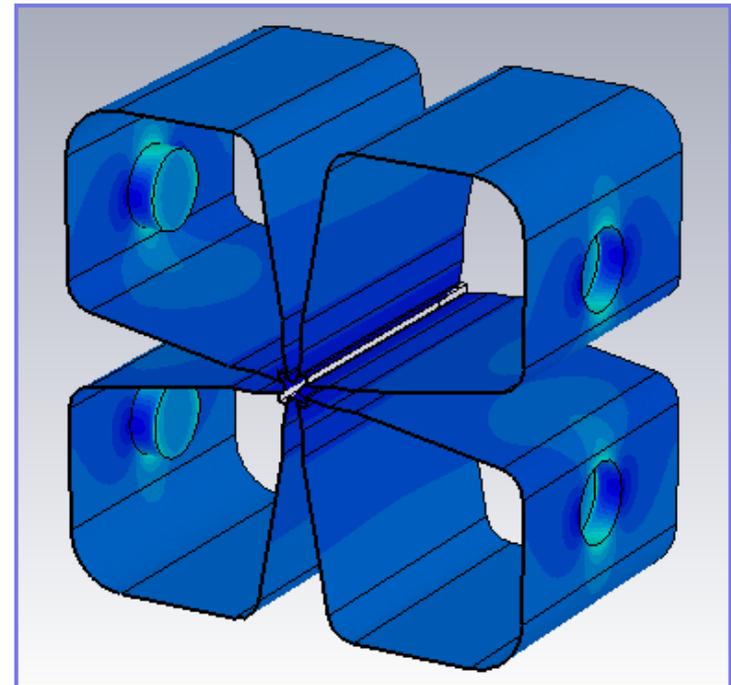
Surface current density



60 mm

20 mm

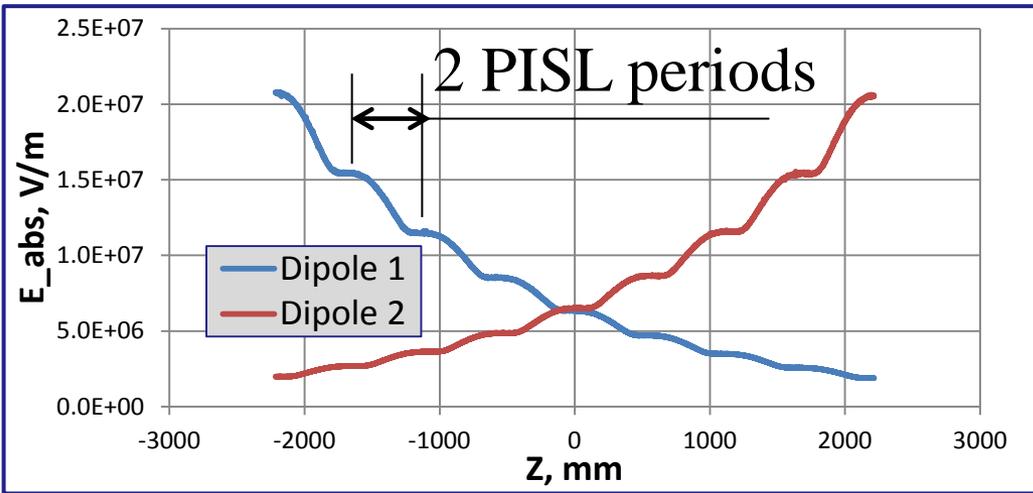
Parameters	PXIE-T
Frequency, MHz	162.495
Frequency shift due tuners, MHz	1.334
Q factor	16115
Q factor drop due tuners, %	-4.1
Power loss per tuner, W	57.7
Tuning sensitivity, kHz/mm	16.7
Nominal tuner intrusion, mm	20
$L_{\max}$ , mm	177.84



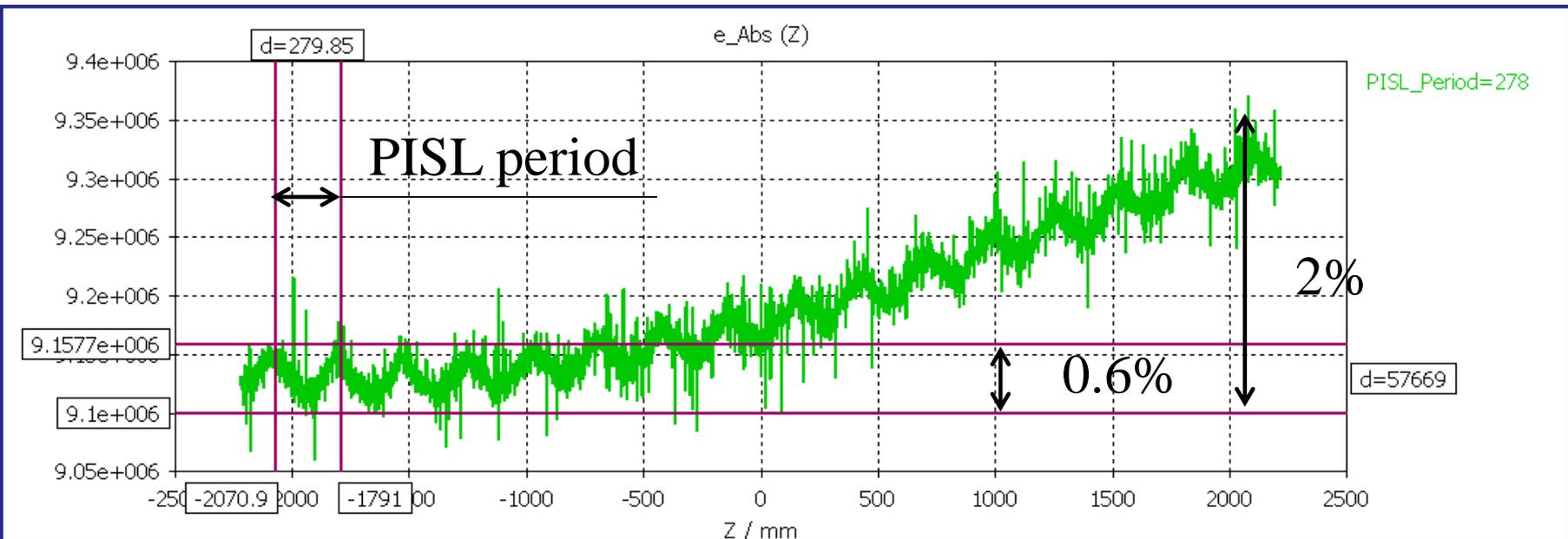




# Field distributions in the vane length model *Project X*

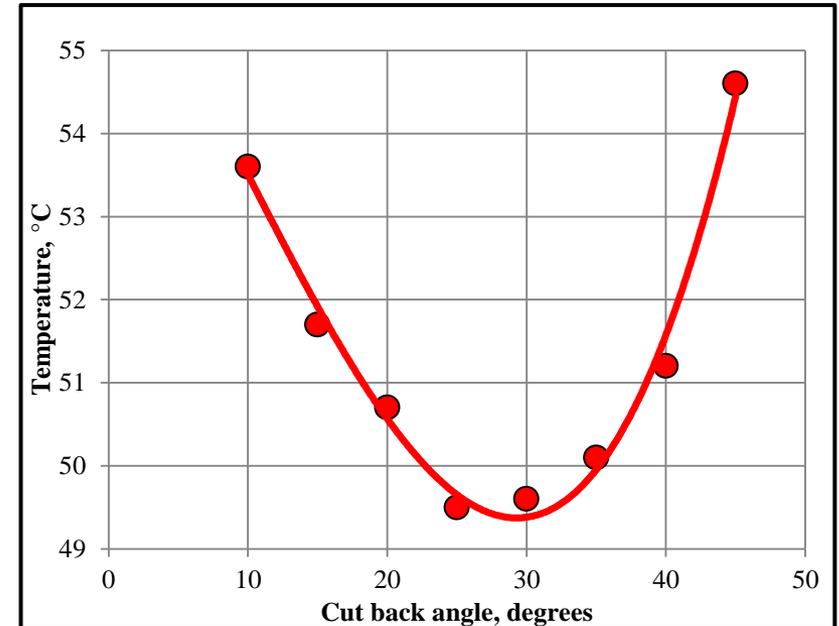
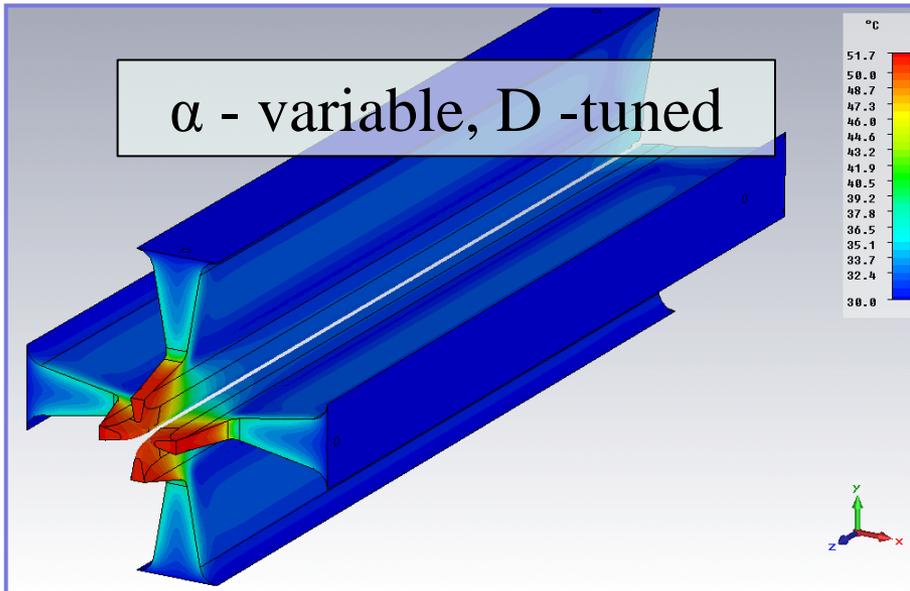
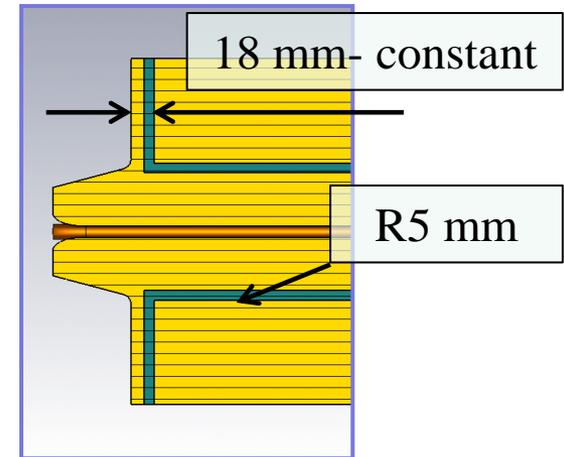
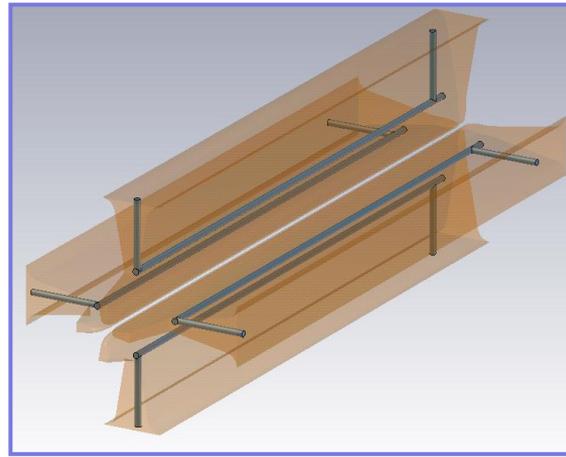
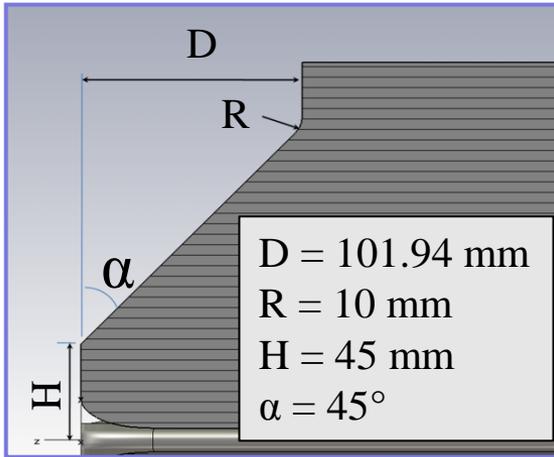


The plots are  $E_{abs}$  along  $x=y=5$  mm line. Modulation of the field distributions is due mostly to the pi-mode rods. The field tilts are due to the asymmetric end terminations. The character of the distortions remains generally the same in the complete RFQ.



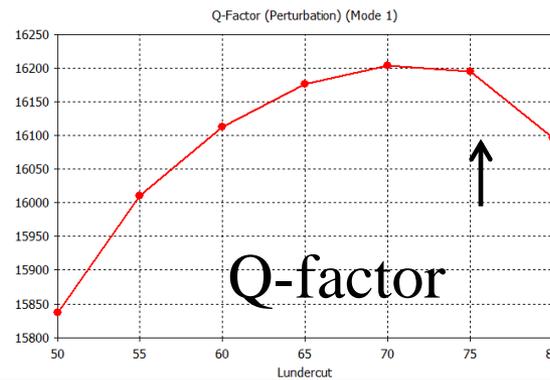
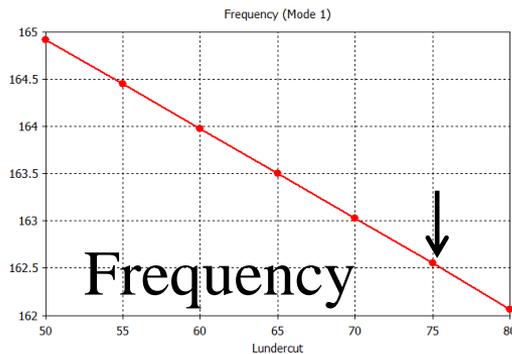
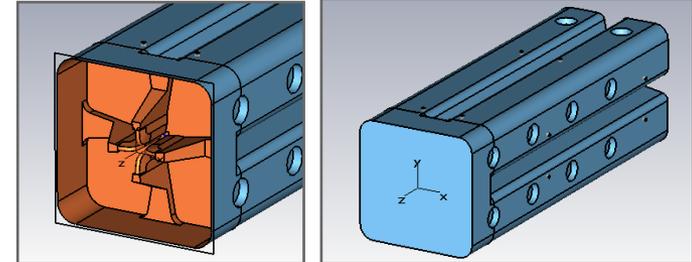
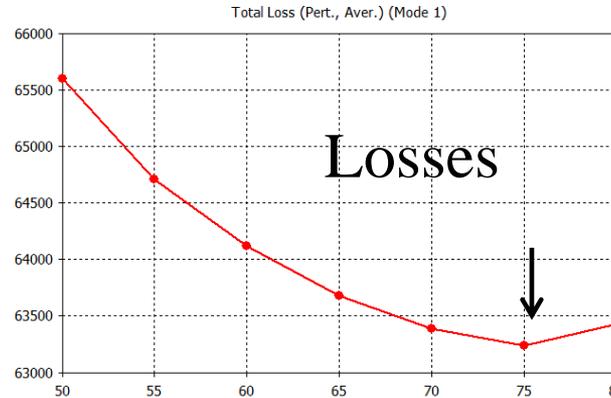
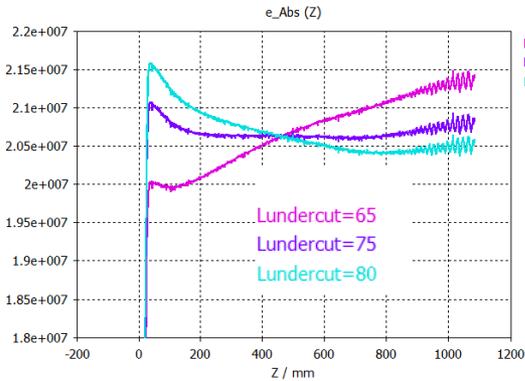


# The cut-back shape



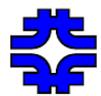


# The standard cut-back tuning

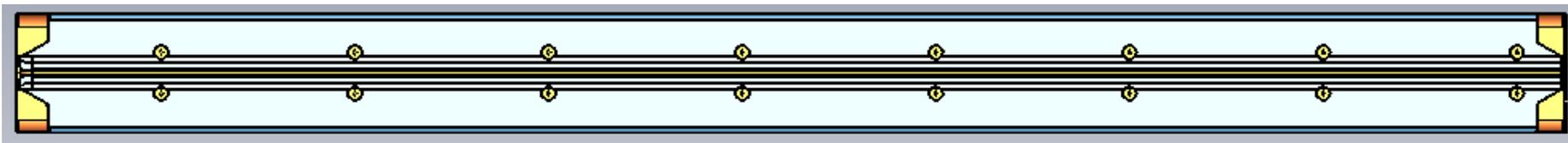


We can tune a frequency of termination using short model. Or flatten a field distribution in a sufficiently long model. Tuning with field tilt control is more accurate, though it requires more resources.

Remarkably that for properly tuned cut-back all parameters are almost optimal. It is not so obvious for full scale model – the changes are too small



# The full scale cut-back tuning



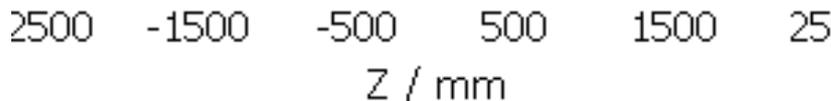
$e_{Abs}(Z)$

Along line  $x=y=5$  mm

CutIn\_Depth=84  
CutIn\_Depth=82.5

Out

In



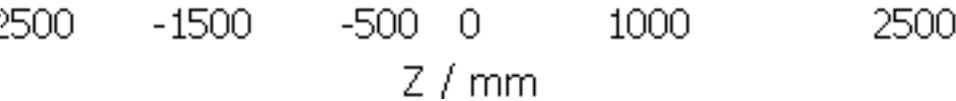
$h_{Abs}(Z)$

Along line  $x=y=50$  mm

CutIn\_Depth=84  
CutIn\_Depth=82.5

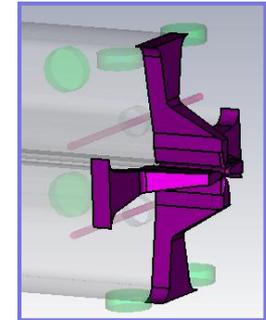
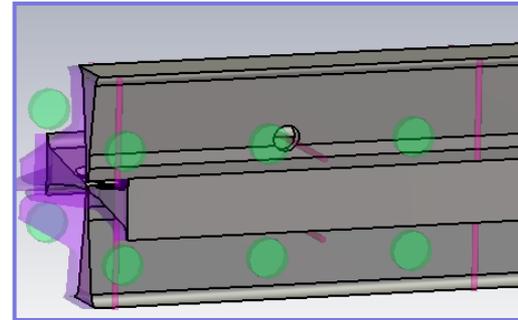
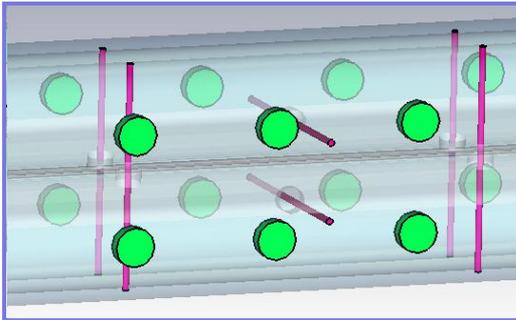
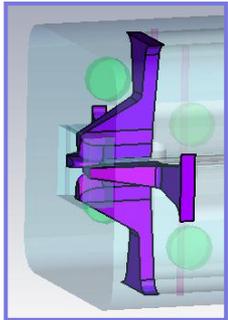
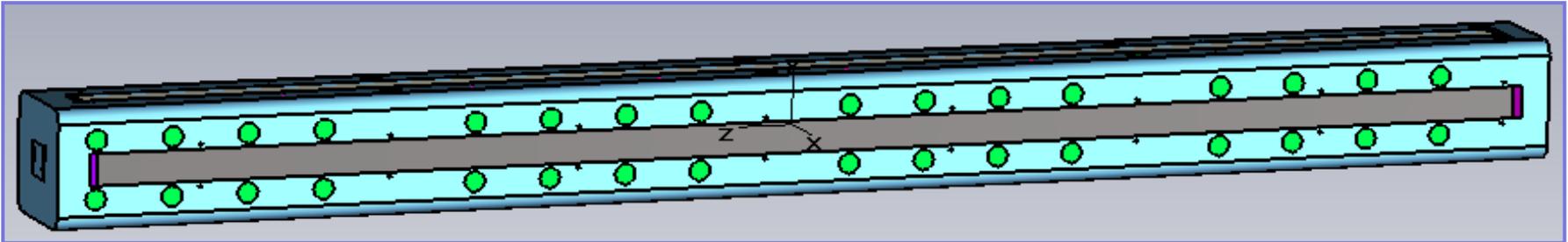
Out

In





# The complete solid model



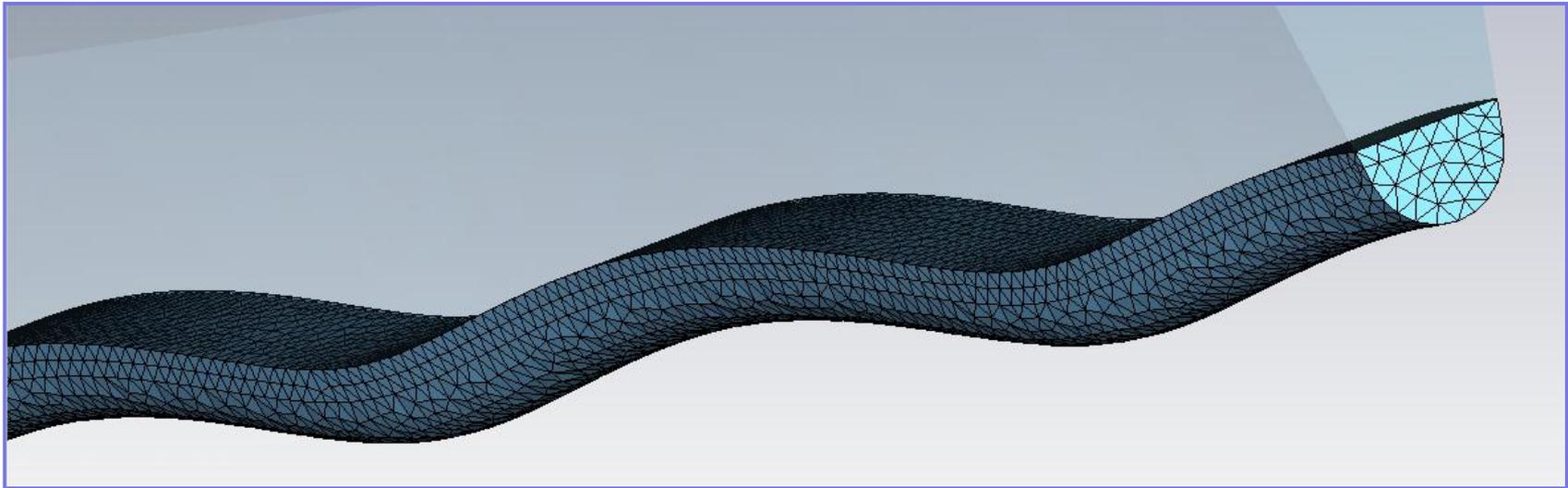
Parameters	PXIE
Frequency, MHz	162.499
Frequency of dipole mode, MHz	181.99
Q factor	14985
Q factor drop due to everything, %	-14.7
Power loss per cut-back, W (In/Out)	336/389
Total power loss, kW	73.8
L_max, mm	172.73

Part	Total, kW	Per unit, W	%
Walls	29.5	-	40
Vanes	31	7764	42
Input cut-backs	1.34	336	1.8
Output cut-backs	1.56	389	2.1
Pi-mode rods	5.53	173	7.5
Tuners	4.79	59.9	6.5



# Vane modulation

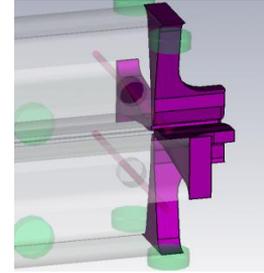
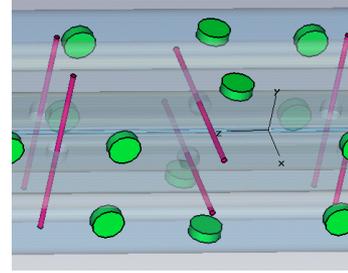
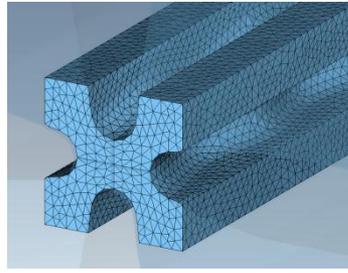
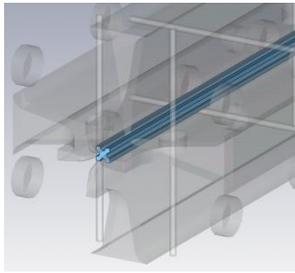
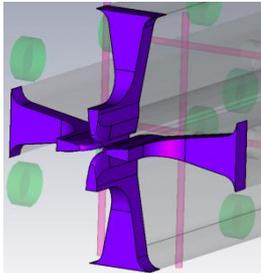
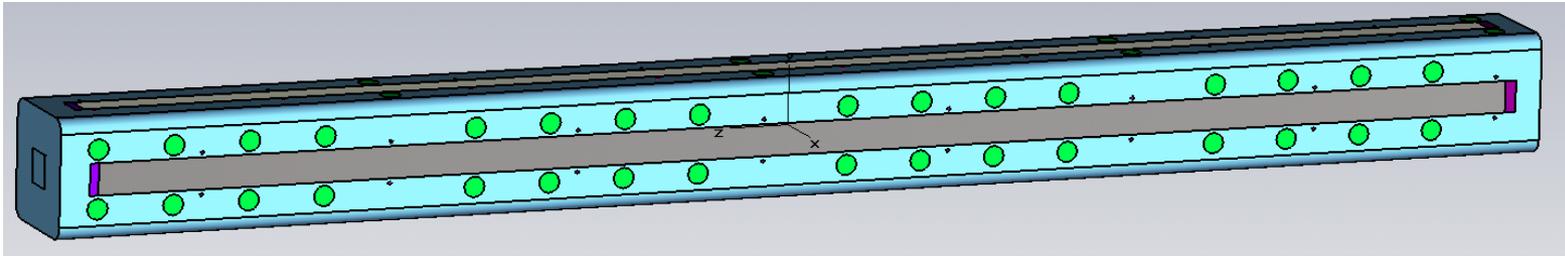
Our computing capability has been increased significantly. We can now create a full scale RFQ model with modulated vanes and solve EM or ES problem.



First of all we can now take a modulation into account during RF design. Also we can now use the “real” fields for beam dynamic simulations.



# Electrodynamics RFQ model

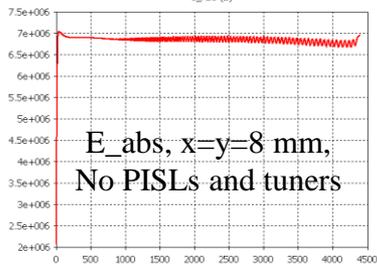


Input matcher. Modulated vane tip.

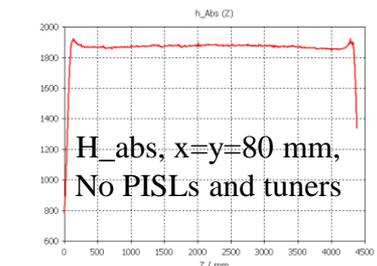
Mesh. 600,000 tets

PISLs and tuners

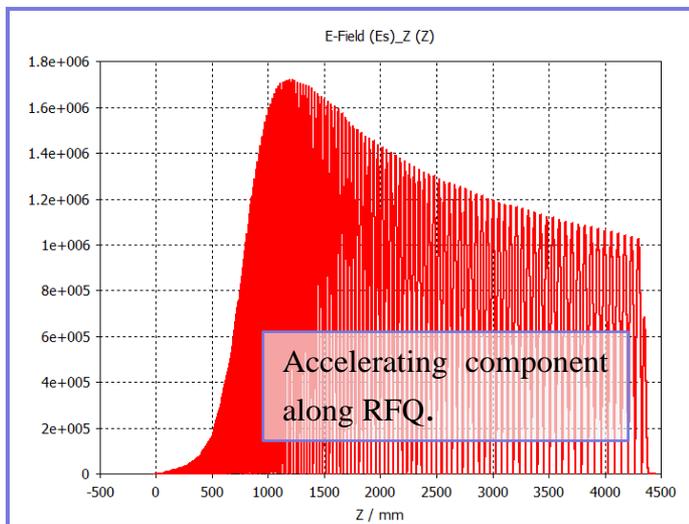
Output termination



$E_{abs}$ ,  $x=y=8$  mm,  
No PISLs and tuners



$H_{abs}$ ,  $x=y=80$  mm,  
No PISLs and tuners

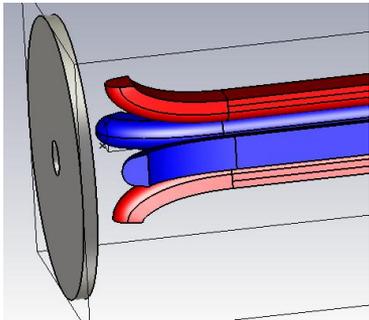
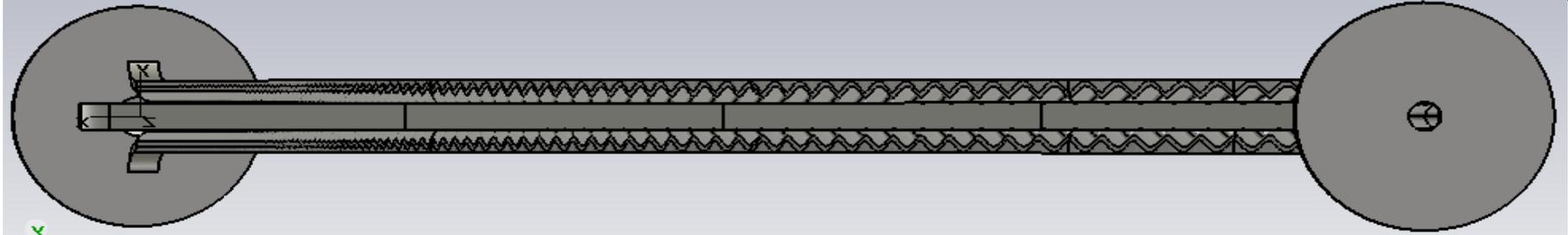


Accelerating component  
along RFQ.

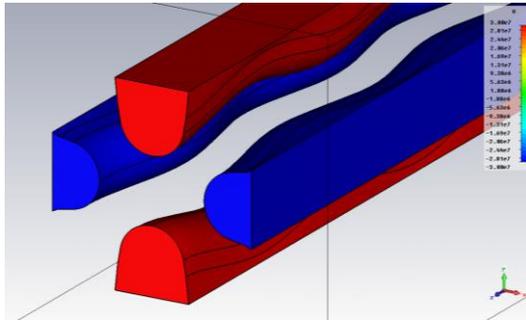
Field distribution in this model reflects influence of many factors – neighboring modes, tuning, stabilizers etc., so the result is never theoretical and may be confusing. On the other hand this is the only approach to analyze real mechanical and tuning errors.



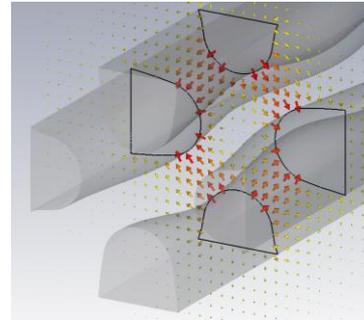
# Electrostatic RFQ model



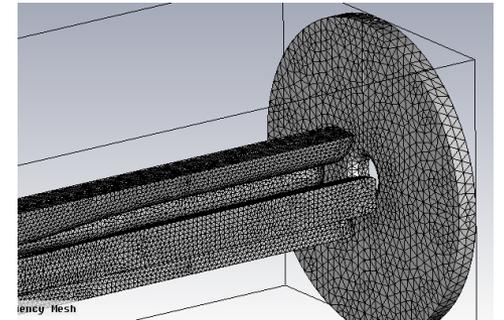
Input matcher with end-wall.



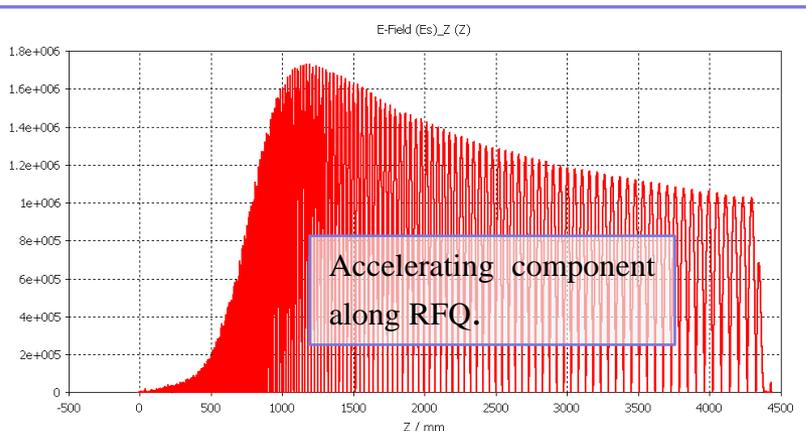
Potentials of  $\pm 30$  kV assigned to the electrodes.



Electrostatic field



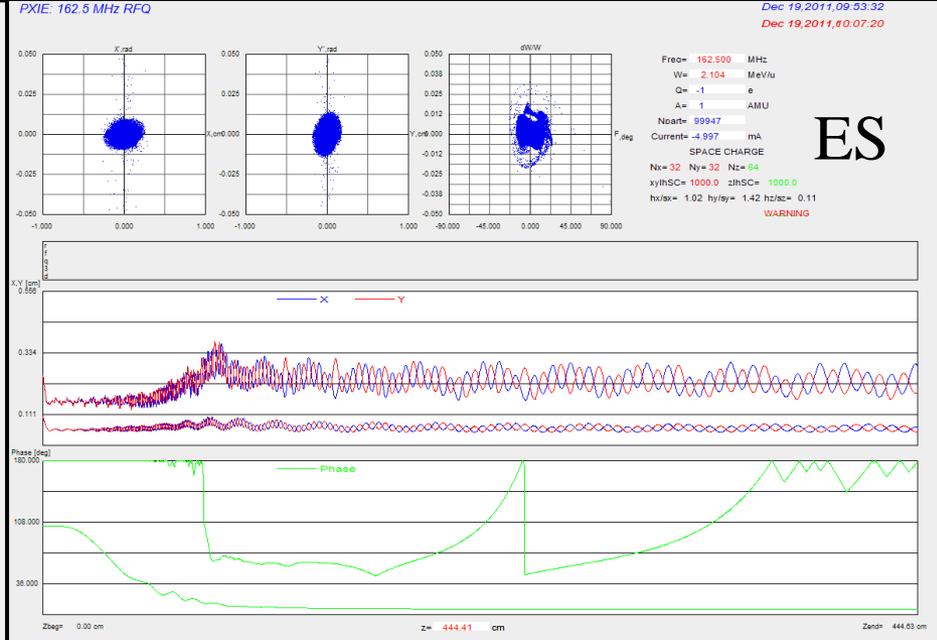
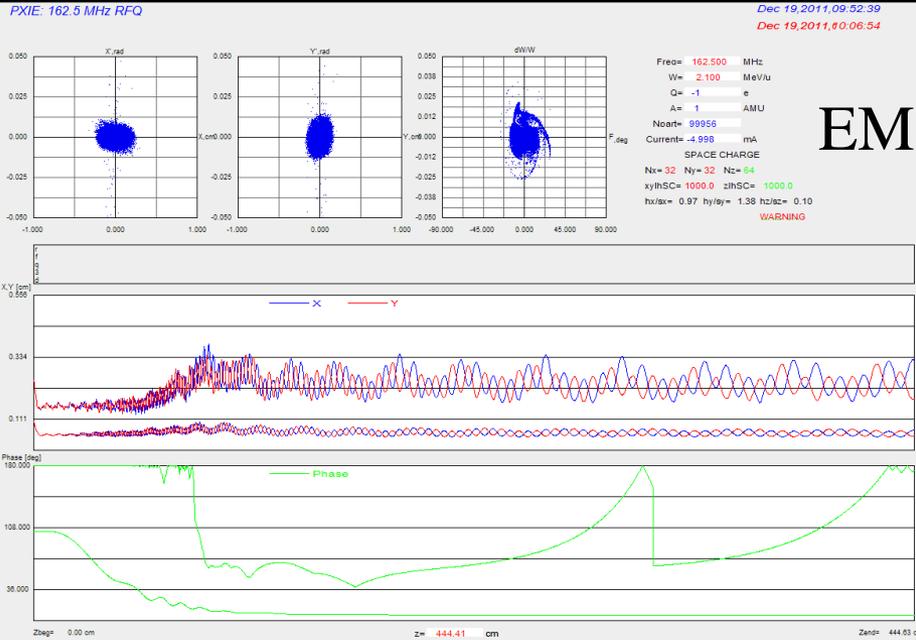
Meshed output termination with end-wall.



The main advantage of the electrostatic model is a designed field distribution – only electrode geometry in paraxial area and electrode potentials matter. And an exact operating frequency can be assigned. But the ES solver uses low frequency mesh which is not very advanced. So, a huge mesh up to 10 M tetrahedrons is needed, and mesh building is very time consuming. The solver itself is very fast though.



# TRACK simulations



	$\alpha$	$\beta$	$4 \epsilon n_{rms}$	Coord.
EM	0.02	0.025	0.054	x
	-0.55	0.012	0.054	y
	0.2	18.35	3.25	z
ES	0.028	0.023	0.054	x
	-0.1	0.012	0.054	y
	0.209	18.99	3.25	z

TRACK units in xy plane:  $\beta$ [cm/mrad],  $\epsilon$ [cm·mrad]  
 TRACK units in z coordinate:  $\beta$ [°·(% of  $\Delta W/W$ )],  $\epsilon$ [keV·ns]

The Twiss parameters at the RFQ exit are close for electrodynamic and electrostatic fields. But detailed particle distribution seems to be different.

Many thanks to Brahim Mustafa for the help with TRACK.



# Conclusion

- RF simulations of RFQ are now well developed and very capable
- A plan is to perform complete RF simulations with full scale model and modulated vane tips.
- Usage of EM and ES fields simulated with complete RFQ model seems to be interesting and promising.